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TPS1H100-Q1 40-V, 100-mΩ Single-Channel Smart High-Side Power Switch

1 Features

- Qualified for automotive applications
- AEC-Q100 Qualified with the following results:
	- Device temperature grade 1: –40°C to 125°C ambient operating temperature range
	- Device HBM ESD classification level H3A
	- Device CDM ESD classification level C4B
- • [Functional](http://www.ti.com/technologies/functional-safety/overview.html) safety capable
	- Documentation available to aid functional safety system design
- Single-channel smart high-side power switch with full diagnostics
	- Version A: open-drain status output
	- Version B: current sense analog output
- Wide operating voltage 3.5 to 40 V
- Very-low standby current, <0.5 µA
- Operating junction temperature, –40 to 150°C
- Input control, 3.3-V and 5-V logic compatible
- • High-accuracy current sense, ±30 mA at 1 A, ±4 mA at 5 mA
- Programmable current limit with external resistor, ±20% at 0.5 A
- Diagnostic enable function for multiplexing of mcu analog or digital interface
- Tested according to AECQ100-12 Grade A, 1 million times Short to GND test
- Electrical transient disturbance immunity certification of ISO7637-2 and ISO16750-2
- **Protection**
	- Overload and short-circuit protection
	- Inductive load negative voltage clamp
	- Undervoltage lockout (UVLO) protection
- Thermal shutdown/swing with self recovery
- Loss of GND, loss of supply protection
- Reverse battery protection with external circuitry
- **Diagnostic**
	- On- and Off-state output open- and short-tobattery detection
	- Overload and short to ground detection and current limit
	- Thermal shutdown/swing detection
- 14-Pin Thermally-enhanced PWP package

2 Applications

- High-side power switch for sub-module
- Power switch for low-wattage lamp
- High-side relays and solenoids
- PLC Digital output power switch
- General resistive, inductive, and capacitive loads

3 Description

The TPS1H100-Q1 device is a fully protected highside power switch, with integrated NMOS power FET and charge pump, targeted for the intelligent control of the variable kinds of resistive, inductive, and capacitive loads. Accurate current sense and programmable current limit features differentiate it from the market.

(1) For all available packages, see the orderable addendum at the end of the data sheet.

Typical Application Schematic

Device Information[\(1\)](#page-0-0)

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4 Revision History

NOTE: Page numbers for previous revisions may differ from page numbers in the current version.

5 Pin Configuration and Functions

Pin Functions

6 Specifications

6.1 Absolute Maximum Ratings

over operating free-air temperature range (unless otherwise noted) $(1)(2)(3)$

(1) Stresses beyond those listed under *Absolute Maximum Ratings* may cause permanent damage to the device. These are stress ratings only, which do not imply functional operation of the device at these or any other conditions beyond those indicated under *Recommended Operating Conditions*. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.

(2) All voltage values are with respect to GND.

(3) Absolute negative voltage on these terminals is not to go below –0.3 V.

(4) Absolute maximum voltage, withstand 48-V load dump voltage for 400 ms.

(5) Reverse polarity condition: t < 60 s, reverse current < Irev1, GND pin 1-kΩ resistor in parallel with diode.
(6) Test condition: V_S = 13.5 V, L = 8 mH, R = 0 Ω, T」= 150°C. FR4 2s2p board, 2- × 70-μm Cu, 2- × 35-μm copper area.

6.2 ESD Ratings

(1) The human-body model is a 107-pF capacitor discharged through a 1.5-k Ω resistor into each terminal.
(2) The charged-device model is tested according to AEC_Q100-011C.

The charged-device model is tested according to AEC_Q100-011C.

6.3 Recommended Operating Conditions

over operating free-air temperature range (unless otherwise noted)

6.4 Thermal Information

(1) For more information about traditional and new thermal metrics, see the *[Semiconductor](http://www.ti.com/lit/pdf/spra953) and IC Package Thermal Metrics* application report.

(2) The thermal data is based on JEDEC standard high-K profile – JESD 51-7. The copper pad is soldered to the thermal land pattern. Also, correct attachment procedure must be incorporated.

- (1) 4-layer board: FR4 2s2p board, 2.8-mil copper (top/bottom), 1.4-mil copper (internal layers). 76.4- × 114.3- × 1.5-mm board size.
- (2) 2-layer board: FR4 2s0p board, 2.8-mil copper (top/bottom). 76.4- × 114.3- × 1.5-mm board size.

Figure 1. RθJA Value vs Copper Area

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6.5 Electrical Characteristics

 $5 V < V_S < 40 V$; $-40°C < T_J < 150°C$ unless otherwise specified

(1) Value is specified by design, not subject to production test.

(2) Value is based on the minimum value of the 10 pcs/3 lots samples.

Electrical Characteristics (continued)

(3) External current-limit accuracy is only applicable to overload conditions greater than 1.5× the current-limit setting.

(4) External current-limit setting is recommended to be higher than 500 mA.

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6.6 Timing Requirements – Current Sense Characteristics(1)

(1) Value specified by design, not subject to production test.

Figure 2. CS Delay Characteristics

Figure 3. Open-Load Blanking Time Characteristics

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6.7 Switching Characteristics

 V_{VS} = 13.5 V, R_{load} = 10 Ω, over operating free-air temperature range (unless otherwise noted)⁽¹⁾

(1) Value specified by design, not subject to production test.

Figure 5. Switching Characteristics Diagram

6.8 Typical Characteristics

All the following data are based on the mean value of the three lots samples, V_{VS} = 13.5 V if not specified.

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Typical Characteristics (continued)

All the following data are based on the mean value of the three lots samples, V_{VS} = 13.5 V if not specified.

Typical Characteristics (continued)

All the following data are based on the mean value of the three lots samples, V_{VS} = 13.5 V if not specified.

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Typical Characteristics (continued)

All the following data are based on the mean value of the three lots samples, $V_{VS} = 13.5$ V if not specified.

7 Detailed Description

7.1 Overview

The TPS1H100-Q1 is a single-channel, fully-protected, high-side power switch with an integrated NMOS power FET and charge pump. Full diagnostics and high-accuracy current-sense features enable intelligent control of the load. A programmable current-limit function greatly improves the reliability of the whole system. The device diagnostic reporting has two versions to support both digital status and analog current-sense output, both of which can be set to the high-impedance state when diagnostics are disabled, for multiplexing the MCU analog or digital interface among devices.

For version A, the digital status report is implemented with an open-drain structure. When a fault condition occurs, it pulls down to GND. A 3.3- or 5-V external pullup is required to match the microcontroller supply level. For version B, high-accuracy current sensing allows a better real-time monitoring effect and more-accurate diagnostics without further calibration. A current mirror is used to source 1 / K of the load current, which is reflected as voltage on the CS pin. K is a constant value across the temperature and supply voltage. The currentsensing function operates normally within a wide linear region from 0 to 4 V. The CS pin can also report a fault by pulling up the voltage of $V_{CS,h}$.

The external high-accuracy current limit allows setting the current limit value by application. It highly improves the reliability of the system by clamping the inrush current effectively under start-up or short-circuit conditions. Also, it can save system costs by reducing PCB trace, connector size, and the preceding power-stage capacity. An internal current limit is also implemented in this device. The lower value of the external or internal current-limit value is applied.

An active drain and source voltage clamp is built in to address switching off the energy of inductive loads, such as relays, solenoids, pumps, motors, and so forth. During the inductive switching-off cycle, both the energy of the power supply (E_{BAT}) and the load (E_{LOAD}) are dissipated on the high-side power switch itself. With the benefits of process technology and excellent IC layout, the TPS1H100-Q1 device can achieve excellent power dissipation capacity, which can help save the external free-wheeling circuitry in most cases. See *[Inductive-Load](#page-18-0) Switching-Off [Clamp](#page-18-0)* for more details.

Short-circuit reliability is critical for smart high-side power-switch devices. The standard of AEC-Q100-012 is to determine the reliability of the devices when operating in a continuous short-circuit condition. Different grade levels are specified according to the pass cycles. This device is qualified with the highest level, Grade A, 1 million times short-to-GND certification.

The TPS1H100-Q1 device can be used as a high-side power switch for a wide variety of resistive, inductive, and capacitive loads, including the low-wattage bulbs, LEDs, relays, solenoids, and heaters.

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7.2 Functional Block Diagram

7.3 Feature Description

7.3.1 Accurate Current Sense

For version B, the high-accuracy current-sense function is internally implemented, which allows a better real-time monitoring effect and more-accurate diagnostics without further calibration. A current mirror is used to source 1 / K of the load current, flowing out to the external resistor between the CS pin and GND, and reflected as voltage on the CS pin.

K is the ratio of the output current and the sense current. It is a constant value across the temperature and supply voltage. Each device was internally calibrated while in production, so post-calibration by users is not required in most cases.

Feature Description (continued)

Ensure the CS voltage is in the linear region (0 to 4 V) during normal operation. Calculate R_{CS} with [Equation](#page-16-0) 1.

$$
R_{CS} = \frac{V_{CS}}{I_{CS}} = \frac{V_{CS} \times K}{I_{out}}
$$
 (1)

Also, when a fault condition occurs, CS works as a diagnostics report pin. When an open load or short to battery occurs in the on-state, V_{CS} almost equals 0. When current limit, thermal shutdown/swing, open load, or short to battery in the off-state occurs, the voltage is pulled up to $V_{CS,h}$. [Figure](#page-17-0) 30 shows a typical current-sense voltage according to the operating conditions, including fault conditions.

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Feature Description (continued)

Figure 30. Voltage Indication on the Current-Sense Pin

Figure 31. Current-Sense and Current-Limit Block Diagram

7.3.2 Programmable Current Limit

A high-accuracy current limit allows higher reliability, which protects the power supply during short circuit or power up. Also, it can save system costs by reducing PCB traces, connector size, and the capacity of the preceding power stage.

Current limit offers protection from overstressing to the load and integrated power FET. Current limit holds the current at the set value, and pulls up the CS pin to $V_{CS,h}$ as a diagnostic report. The two current-limit thresholds are:

• External programmable current limit -- An external resistor is used to convert a proportional load current into a voltage, which is compared with an internal reference voltage, $V_{th,cl}$. When the voltage on the CL pin exceeds $V_{th, cl}$, a closed loop steps in immediately. V_{GS} voltage regulates accordingly, leading to the V_{ds} voltage regulation. When the closed loop is set up, the current is clamped at the set value. The external programmable current limit provides the capability to set the current-limit value by application.

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Feature Description (continued)

• Internal current limit -- The internal current limit is fixed and typically 10 A. To use the internal current limit for large-current applications, tie the CL pin directly to the device GND.

Both the internal current limit (I_{lim,nom}) and external programmable current limit are always active when V_{VS} is powered and IN is high. The lower one (of I_{lim,nom} and the external programmable current limit) is applied as the actual current limit.

Note that if a GND network is used (which leads to the level shift between the device GND and board GND), the CL pin must be connected with device GND. Calculate R_{Cl} with [Equation](#page-18-1) 2.

$$
I_{CL} = \frac{V_{CL,th}}{R_{CL}} = \frac{I_{out}}{K_{CL}} \rightarrow R_{CL} = \frac{V_{CL,th} \times K_{CL}}{I_{out}}
$$
(2)

For better protection from a hard short-to-GND condition (when V_S and input are high and a short to GND happens suddenly), an open-loop fast-response behavior is set to turn off the channel, before the current-limit closed loop is set up. The open-loop response time is around 1 µs. With this fast response, the device can achieve better inrush-suppression performance.

7.3.3 Inductive-Load Switching-Off Clamp

When an inductive load is switching off, the output voltage is pulled down to negative, due to the inductance characteristics. The power FET may break down if the voltage is not clamped during the current-decay period. To protect the power FET in this situation, internally clamp the drain-to-source voltage, namely $V_{DS,clamp}$, the clamp diode between the drain and gate.

$$
V_{DS,clamp} = V_{BAT} - V_{OUT} \tag{3}
$$

During the current-decay period (T_{DECAY}) , the power FET is turned on for inductance-energy dissipation. Both the energy of the power supply (E_{BAT}) and the load (E_{LOAD}) are dissipated on the high-side power switch itself, which is called E_{HSD} . If resistance is in series with inductance, some of the load energy is dissipated in the resistance.

$$
E_{HSD} = E_{BAT} + E_{LOAD} = E_{BAT} + E_L - E_R
$$
\n
$$
\tag{4}
$$

From the high-side power switch's view, E_{HSD} equals the integration value during the current-decay period.

$$
E_{\text{HSD}} = \int_{0}^{T_{\text{DECAY}}} V_{\text{DS,clamp}} \times I_{\text{OUT}}(t) dt
$$
\n
$$
L_{\text{L}} \left(\frac{R \times I_{\text{OUT}(MAX)} + |V_{\text{OUT}}|}{R \times I_{\text{OUT}(MAX)}} + |V_{\text{OUT}}|} \right)
$$
\n(5)

$$
T_{DECAY} = \frac{L}{R} \times \ln\left(\frac{R \times l_{OUT(MAX)} + |V_{OUT}|}{|V_{OUT}|}\right)
$$
\n
$$
E_{HSD} = L \times \frac{V_{BAT} + |V_{OUT}|}{R^2} \times \left[R \times l_{OUT(MAX)} - |V_{OUT}| \ln\left(\frac{R \times l_{OUT(MAX)} + |V_{OUT}|}{|V_{OUT}|}\right)\right]
$$
\n(7)

 $|V_{\text{OUT}}|$

When R approximately equals 0, E_{HSD} can be given simply as:

$$
E_{HSD} = \frac{1}{2} \times L \times I_{OUT(MAX)}^2 \frac{V_{BAT} + |V_{OUT}|}{R^2}
$$
 (8)

(7)

Feature Description (continued)

Figure 32. Driving Inductive Load

Figure 33. Inductive-Load Switching-Off Diagram

As discussed previously, when switching off, battery energy and load energy are dissipated on the high-side power switch, which leads to the large thermal variation. For each high-side power switch, the upper limit of the maximum safe power dissipation depends on the device intrinsic capacity, ambient temperature, and board dissipation condition. TI provides the upper limit of single-pulse energy that devices can tolerate under the test condition: V_{VS} = 13.5 V, inductance from 0.1 mH to 400 mH, R = 0 Ω , FR4 2s2p board, 2- × 70-µm copper, 2- × 35 -µm copper, thermal pad copper area 600 mm².

For one dedicated inductance, see [Figure](#page-19-0) 34. If the maximum switching-off current is lower than the current value shown on the curve, the internal clamp function can be used for the demagnetization energy dissipation. If not, external free-wheeling circuitry is necessary for device protection.

Feature Description (continued)

Figure 34. Maximum Current vs Inductance Range

7.3.4 Full Protections and Diagnostics

[Table](#page-20-0) 1 is when DIAG_EN enabled. When DIAG_EN is low, current sense or ST is disabled accordingly. The output is in high-impedance mode. Refer to [Table](#page-20-1) 2 for details.

Table 1. Fault Table

(1) Need external pullup resistor during off-state

Table 2. DIAG_EN Logic Table

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7.3.4.1 Short-to-GND and Overload Detection

In the on state, the short-to-GND fault is reported as the low status output or $V_{CS,h}$ on CS, when a current limit is triggered. The lower one of the internal and external set values is applied for the actual current limit. It is in autorecovery when the fault condition is cleared. If not cleared, thermal shutdown triggers to protect the power FET.

7.3.4.2 Open-Load Detection

In the on state for version A, if the current flowing through the output is less than $I_{ol,on}$, the device recognizes an open-load fault. For version B, faults are diagnosed by reading the voltage on the CS pin and judged by the user. A benefit of high-accuracy current sense down to a verylow current range, this device can achieve a very low open-load detection threshold, which correspondingly expands the normal operation region. TI suggests 10 mA as the upper limit for the open-load detection threshold and 25 mA as the lower limit for the normal operation current. In [Figure](#page-21-0) 35, the recommended open-load detection region is shown as the dark-shaded region and the light-shaded region is for normal operation. As a guideline, do not overlap these two regions.

Figure 35. On-State Open-Load Detection and Normal-Operation Diagram

In the off state, if a load is connected, the output voltage is pulled to 0 V. In the case of an open load, the output voltage is close to the supply voltage, $V_S - V_{OUT} < V_{ol, off}$. For version A, the ST pin goes low to indicate the fault to the MCU. For version B, the CS pin is pulled up to $V_{CS,h}$. There is always a leakage current $I_{ol,off}$ present on the output, due to the internal logic control path or external humidity, corrosion, and so forth. Thus, TI recommends an external pullup resistor to offset the leakage current. This pullup current should be less than the output load current to avoid false detection in the normal operation mode. To reduce the standby current, TI recommends always to use a switch in series with? the pullup resistor. TI recommends $R_{\text{pu}} \le 15$ k Ω .

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7.3.4.3 Short-to-Battery Detection

Short-to-battery detectioin has the same detection mechanism and behavior as open-load detection, both in the on-state and off-state. See the fault truth table, [Table](#page-20-0) 1, for more details. In the on-state, the reverse current flows through the FET instead of the body diode, leading to less power dissipation. Thus, the worst case for offstate is when reverse current occurs. In the off-state, if $\rm V_{OUT}$ – $\rm V_{VS}$ < $\rm V_F$, short to battery can be detected. ($\rm V_F$ is the body diode forward voltage and typically 0.7 V.) However, the reverse current does not occur. If $\rm V_{OUT}$ – $\rm V_{VS}$ > V_F , short to battery can be detected, and the reverse current should be lower than I_{rev2} to ensure the survival of the device. TI recommends switching on the input for lower power dissipation or the reverse block circuitry for the supply. See *Reverse Current [Protection](#page-27-0)* for more external protection circuitry information.

7.3.4.4 Reverse-Polarity Detection

Reverse-polarity detection has the same detection mechanism and behavior as open-load detection, both in the on-state and off-state. See the fault truth table, [Table](#page-20-0) 1, for more details. In the on-state, the reverse current flows through the FET instead of the body diode, leading to less power dissipation. Thus, the worst case off-state is when reverse current occurs. In off-state, the reverse current should be lower than I_{rev1} to ensure the survival of the device. See *Reverse Current [Protection](#page-27-0)* for more external protection circuitry information.

7.3.4.5 Thermal Protection Behavior

Both the absolute temperature thermal shutdown and the dynamic temperature thermal swing diagnostic and protection are built into the device to increase the maximum reliability of the power FET. Thermal swing is active when the temperature of the power FET is increasing sharply, that is $\Delta T = T_{DMOS} - T_{Logic} > T_{sw}$, then the output is shut down, and the ST pin goes low, or the CS pin is pulled up to $\rm V_{CS,h}$. It auto-recovers and clears the fault signal until ΔT = T_{DMOS} – T_{Logic} < T_{sw} – T_{hys}. Thermal swing function improves device reliability against repetitive fast thermal variation, as shown in [Figure](#page-23-0) 37. Multiple thermal swings are triggered before thermal shutdown happens. Thermal shutdown is active when absolute temperature $T > T_{SD}$. When active, the output is shut down, and the ST pin goes low, or the CS pin is pulled up to V_{CS,h}. The output is auto-recovered when T < T_{SD} – T_{hys}; the current limit is reduced to I_{lim,tsd}, or half of the programmable current limit value, to avoid repeated thermal shutdown. However, the thermal shutdown fault signal and half-current limit value are not cleared until the junction temperature decreases to less than $T_{SD,rst}$.

Figure 37. Thermal Behavior

7.3.4.6 UVLO Protection

The device monitors the supply voltage V_{VS} to prevent unpredicted behaviors in the event that the supply voltage is too low. When the supply voltage falls down to V_{VS,UVF}, the output stage is shut down automatically. When the supply rises up to $\mathsf{V}_{\mathsf{VS},\mathsf{UVR}},$ the device turns on.

7.3.4.7 Loss of GND Protection

When loss of GND occurs, output is turned off regardless of whether the input signal is high or low.

Case 1 (loss of device GND): Loss of GND protection is active when the Tab, I_{C_GND}, and current limit GND are one trace connected to the board GND, as shown in [Figure](#page-24-0) 38. Tab floating is also a choice.

Figure 38. Loss of Device GND

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Case 2 (loss of module GND): When the whole ECU module GND is lost, protections are also active. At this condition, the load GND remains connected.

Figure 39. Loss of Module GND

7.3.4.8 Loss of Power Supply Protection

When loss of supply occurs, output is turned off regardless of whether the input is high or low. For a resistive or capacitive load, loss-o-supply protection is easy to achieve due to no more power. The worst case is a charged inductive load. In this case, the current is driven from all of the IOs to maintain the inductance output loop. TI recommends either the MCU serial resistor plus the GND network (diode and resistor in parallel) or external freewheeling circuitry.

Figure 40. Loss of Battery

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7.3.4.9 Reverse Current Protection

Method 1: Block diode connected with V_S. Both the device and load are protected when in reverse polarity.

Figure 41. Reverse Protection With Block Diode

Method 2 (GND network protection): Only the high-side device is protected under this connection. The load reverse loop is limited by the load itself. Note when reverse polarity happens, the continuous reverse current through the power FET should be less than I_{rev} . Of the three types of ground pin networks, TI strongly recommends type 3 (the resistor and diode in parallel). No matter what types of connection are between the device GND and the board GND, if a GND voltage shift happens, ensure the following proper connections for the normal operation:

- Leave the NC pin floating or connect to the device GND. TI recommends to leave floating.
- Connect the current limit programmable resistor to the device GND.

Figure 42. Reverse Protection With GND Network

• **Type 1 (resistor):** The higher resistor value contributes to a better current limit effect when the reverse battery or negative ISO pulses. However, it leads to higher GND shift during normal operation mode. Also, consider the resistor's power dissipation.

$$
R_{GND} \leq \frac{V_{GNDshift}}{I_{nom}}
$$

$$
R_{GND} \geq \frac{(-V_{CC})}{(-I_{GND})}
$$

(9)

where

- V_{GNDshift} is the maximum value for the GND shift, determined by the HSD and microcontroller. TI suggests a value ≤ 0.6 V .
- I_{nom} is the nominal operating current.
- $-V_{CC}$ is the maximum reverse voltage seen on the battery line.
- –IGND is the maximum reverse current the ground pin can withstand, which is available in the *[Absolute](#page-3-1) [Maximum](#page-3-1) Ratings*. (10)

If multiple high-side power switches are used, the resistor can be shared among devices.

• **Type 2 (diode):** A diode is needed to block the reverse voltage, which also brings a ground shift (≈ 600 mV).

However, an inductive load is not acceptable to avoid an abnormal status when switching off.

• **Type 3 (resistor and diode in parallel (recommended)):** A peak negative spike may occur when the inductive load is switching off, which may damage the HSD or the diode. So, TI recommends a resistor in parallel with the diode when driving an inductive load. The recommended selection are 1-kΩ resistor in parallel with an $I_F > 100$ -mA diode. If multiple high-side switches are used, the resistor and diode can be shared among devices.

7.3.4.10 Protection for MCU I/Os

In many conditions, such as the negative ISO pulse, or the loss of battery with an inductive load, a negative potential on the device GND pin may damage the MCU I/O pins [more likely, the internal circuitry connected to the pins]. Therefore, the serial resistors between MCU and HSD are required.

Also, for proper protection against loss of GND, TI recommends 4.7 kΩ when using 3.3-V MCU I/Os; 10 kΩ is for 5-V applications.

Figure 43. MCU IO Protections

7.3.5 Diagnostic Enable Function

The diagnostic enable pin, DIAG_EN, offers multiplexing of the microcontroller diagnostic input for current sense or digital status, by sharing the same sense resistor and ADC line or I/O port among multiple devices.

In addition, during the output-off period, the diagnostic disable function lowers the current consumption for the standby condition. The three working modes in the device are normal mode, standby mode, and standby mode with diagnostic. If off-state power saving is required in the system, the standby current is <500 nA with DIAG_EN low. If the off-state diagnostic is required in the system, the typical standby current is around 1 mA with DIAG EN high.

7.4 Device Functional Modes

7.4.1 Working Mode

The three working modes in the device are normal mode, standby mode, and standby mode with diagnostic. If an off-state power saving is required in the system, the standby current is less than 500 nA with DIAG_EN low. If an off-state diagnostic is required in the system, the typical standby current is around 1 mA with DIAG_EN high. Note that to enter standby mode requires IN low and $t > t_{off,deg}$ t_{off,deg} is the standby-mode deglitch time, which is used to avoid false triggering. [Figure](#page-30-1) 44 shows a work-mode state-machine state diagram.

Figure 44. Work-Mode State Machine

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8 Application and Implementation

NOTE

Information in the following applications sections is not part of the TI component specification, and TI does not warrant its accuracy or completeness. TI's customers are responsible for determining suitability of components for their purposes. Customers should validate and test their design implementation to confirm system functionality.

8.1 Application Information

The following discussion notes how to implement the device to distinguish the different fault modes and implement a ? transient-pulse immunity test.

In some applications, open load, short to battery, and short to GND must be distinguished from each other. This requires two steps.

8.2 Typical Application

[Figure](#page-31-3) 45 shows an example of how to design the external circuitry parameters.

Figure 45. Typical Application Circuitry

Typical Application (continued)

8.2.1 Design Requirements

- V_S range from 9 V to 16 V
- Nominal current of 2 A
- Current sense for fault monitoring
- Expected current limit value of 5 A
- Full diagnostics with 5-V MCU
- Reverse protection with GND network

8.2.2 Detailed Design Procedure

The R_{CS}, V_{CS} linear region is from 0 to 4 V. To keep the 2-A nominal current in the 0- to 3-V range, calculate the R_{CS} as in [Equation](#page-32-0) 11. To achieve better current sense accuracy, a 1% accuracy or better resistor is preferred.

$$
R_{CS} = \frac{V_{CS}}{I_{CS}} = \frac{V_{CS} \times K}{I_{OUT}} = \frac{3 \times 500}{2} = 750 \ \Omega
$$
\n(11)
\n
$$
V_{CL,th}
$$
 is the current-limit internal threshold, 1.233 V. To set the programmable current limit value at 5 A,
\nlate the R_{CL} as in Equation 12.
\n
$$
R_{CI} = \frac{V_{cl,th} \times K_{CL}}{I_{IC}} = \frac{1.233 \times 2000}{1.233 \times 2000} = 493.2 \ \Omega
$$

 R_{CL} , $V_{CL,th}$ is the current-limit internal threshold, 1.233 V. To set the programmable current limit value at 5 A, calculate the R_{CL} as in [Equation](#page-32-1) 12.

$$
R_{CL} = \frac{V_{cl,th} \times K_{CL}}{I_{OUT}} = \frac{1.233 \times 2000}{5} = 493.2 \ \Omega
$$
\n(12)

TI recommends R_{SFR} = 10 kΩ for 5-V MCU.

TI recommends a 1-kΩ resistor and 200-V, 0.2-A diode for the GND network.

8.2.2.1 Distinguishing of Different Fault Modes

Some applications require that open load, short to battery, and short to GND can be distinguished from each other. This requires two steps:

- 1. In the on-state, for the current-sense version device (version B), on-state open load and short to battery are recognized as an extremely-low voltage level on the current-sense pin, whereas short to GND is reported as a pulled-up voltage $V_{CS,h}$. Therefore, the user can find a short to GND (see [Figure](#page-33-0) 46).
- 2. If reported as an on-state open-load or short-to-battery fault in the first step, turn off the input signal. In the off-state, with an external pulldown resistor, open load and short to battery can be easily distinguished. When the output pulls down, the short to battery is still reported as an off-state fault condition, whereas the open load is ignored.

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Typical Application (continued)

Figure 46. Step 1: Short-to-GND Detection in the On-State

Figure 47. Step 2: Short-to-Battery Detection in the Off-State

8.2.2.2 AEC Q100-012 Test Grade A Certification

Short-circuit reliability is critical for smart high-side power switch devices. The AEC-Q100-012 standard is used to determine the reliability of the devices when operating in a continuous short-circuit condition. Different grade levels are specified according to the pass cycles. This device is qualified with the highest level, Grade A, 1 million times short-to-GND certification.

Three test modes are defined in the AEC Q100-012 standard. See [Table](#page-34-0) 3 for cold repetitive short-circuit test – long pulse, cold repetitive short-circuit test – short pulse, and hot repetitive short-circuit test.

Typical Application (continued)

Different grade levels are specified according to the pass cycles. The TPS1H100-Q1 device gets the certification of Grade A level, 1 million short-to-GND cycles, which is the highest test standard in the market.

Grade	Number of Cycles	Lots, Samples Per Lot	Number of Fails
A	>1000000	3, 10	
B	>300000 to 1000000	3, 10	O
C	>100000 to 300000	3, 10	
D	>30000 to 100000	3, 10	
F	>10000 to 30000	3, 10	0
F	>3000 to 10000	3, 10	O
G	>1000 to 3000	3, 10	
н	300 to 1000	3, 10	0
	300	3, 10	

Table 4. Grade Levels

8.2.2.3 EMC Transient Disturbances Test

Due to the severe electrical conditions in the automotive environment, immunity capacity against electrical transient disturbances is required, especially for a high-side power switch, which is connected directly to the battery. Detailed test requirements are in accordance with the ISO 7637-2:2011 and ISO 16750-2:2010 standards. The TPS1H100-Q1 device is tested and certificated by a third-party organization.

Table 5. ISO 7637-2:2011(E) in 12-V System(1)(2)(3)(4)

(1) Tested both under input low condition and high condition.

(2) Considering the worst test condition, it is tested without any filter capacitors in V_S and V_{OUT}.
(3) GND pin network is a 1-kΩ resistor in parallel with a diode BAS21-7-F.

GND pin network is a 1-kΩ resistor in parallel with a diode BAS21-7-F.

 (4) Status II: The function does not perform as designed during the test, but returns automatically to normal operation after the test.

Table 6. ISO 16750-2:2010(E) Load Dump Test B in 12-V System(1)(2)(3)(4)(5)

(1) Tested both under input low condition and high condition. [DIAG_EN, IN, and VS are all classified as inputs. Which one?

(2) Considering the worst test condition, the device is tested without any filter capacitors on VS and OUT.
(3) The GND pin network is a 1-k Ω resistor in parallel with a diode BAS21-7-F.

The GND pin network is a 1-kΩ resistor in parallel with a diode BAS21-7-F.

(4) Status II: The function does not perform as designed during the test, but returns automatically to normal operation after the test.

(5) Select a 45-V external suppressor.

[TPS1H100-Q1](http://www.ti.com/product/tps1h100-q1?qgpn=tps1h100-q1)

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8.2.3 Application Curves

[Figure](#page-35-0) 48 shows a test example of initial short-circuit inrush-current limit. Test conditions: $V_S = 13.5$ V, input is from low to high, load is short-to-GND or with a 470-µF capacitive load, external current limit is 2 A. CH1 is the output current. CH3 is the input step.

[Figure](#page-35-0) 49 shows a test example of a hard short-circuit inrush-current limit. Test conditions: $V_{\rm SI}$ = 13.5 V, input is high, load is 5 µH + 100 mΩ, external current limit is 1 A. A short to GND suddenly happens.

9 Power Supply Recommendations

The device is qualified for both automotive and industrial applications. The normal power supply connection is a 12-V automotive system or 24-V industrial system. The supply voltage should be within the range specified in the *[Recommended](#page-3-3) Operating Conditions*.

10 Layout

10.1 Layout Guidelines

To prevent thermal shutdown, T_J must be less than 150°C. If the output current is very high, the power dissipation may be large. The HTSSOP package has good thermal impedance. However, the PCB layout is very important. Good PCB design can optimize heat transfer, which is absolutely essential for the long-term reliability of the device.

- Maximize the copper coverage on the PCB to increase the thermal conductivity of the board. The major heatflow path from the package to the ambient is through the copper on the PCB. Maximum copper is extremely important when there are not any heat sinks attached to the PCB on the other side of the board opposite the package.
- Add as many thermal vias as possible directly under the package ground pad to optimize the thermal conductivity of the board.
- All thermal vias should either be plated shut or plugged and capped on both sides of the board to prevent solder voids. To ensure reliability and performance, the solder coverage should be at least 85%.

10.2 Layout Example

10.2.1 Without a GND Network

Without a GND network, tie the thermal pad directly to the board GND copper for better thermal performance.

Figure 50. Layout Without a GND Network

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TEXAS

Layout Example (continued)

10.2.2 With a GND Network

With a GND network, tie the thermal pad with a single trace through the GND network to the board GND copper.

Figure 51. Layout With a GND Network

10.3 Thermal Considerations

This device possesses thermal shutdown (TSD) circuitry as a protection from overheating. For continuous normal operation, the junction temperature should not exceed the thermal-shutdown trip point. If the junction temperature exceeds the thermal-shutdown trip point, the output turns off. When the junction temperature falls below the thermal-shutdown trip point, the output turns on again.

Calculate the power dissipated by the device according to [Equation](#page-37-1) 13.

$$
P_T = I_{OUT}^2 \times R_{DSON} + V_S \times I_{nom}
$$

where

• P_T = Total power dissipation of the device (13)

After determining the power dissipated by the device, calculate the junction temperature from the ambient temperature and the device thermal impedance.

 $T_{J} = T_{A} + R_{AJA} \times P_{T}$

 (14)

11 Device and Documentation Support

11.1 Receiving Notification of Documentation Updates

To receive notification of documentation updates, navigate to the device product folder on ti.com. In the upper right corner, click on *Alert me* to register and receive a weekly digest of any product information that has changed. For change details, review the revision history included in any revised document.

11.2 Community Resources

TI E2E™ [support](http://e2e.ti.com) forums are an engineer's go-to source for fast, verified answers and design help — straight from the experts. Search existing answers or ask your own question to get the quick design help you need.

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11.3 Trademarks

E2E is a trademark of Texas Instruments. All other trademarks are the property of their respective owners.

11.4 Electrostatic Discharge Caution

These devices have limited built-in ESD protection. The leads should be shorted together or the device placed in conductive foam during storage or handling to prevent electrostatic damage to the MOS gates.

11.5 Glossary

[SLYZ022](http://www.ti.com/lit/pdf/SLYZ022) — *TI Glossary*.

This glossary lists and explains terms, acronyms, and definitions.

12 Mechanical, Packaging, and Orderable Information

The following pages include mechanical, packaging, and orderable information. This information is the most current data available for the designated devices. This data is subject to change without notice and revision of this document. For browser-based versions of this data sheet, refer to the left-hand navigation.

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PACKAGING INFORMATION

(1) The marketing status values are defined as follows:

ACTIVE: Product device recommended for new designs.

LIFEBUY: TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.

NRND: Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

PREVIEW: Device has been announced but is not in production. Samples may or may not be available.

OBSOLETE: TI has discontinued the production of the device.

⁽²⁾ RoHS: TI defines "RoHS" to mean semiconductor products that are compliant with the current EU RoHS requirements for all 10 RoHS substances, including the requirement that RoHS substance do not exceed 0.1% by weight in homogeneous materials. Where designed to be soldered at high temperatures. "RoHS" products are suitable for use in specified lead-free processes. TI may reference these types of products as "Pb-Free".

RoHS Exempt: TI defines "RoHS Exempt" to mean products that contain lead but are compliant with EU RoHS pursuant to a specific EU RoHS exemption.

Green: TI defines "Green" to mean the content of Chlorine (CI) and Bromine (Br) based flame retardants meet JS709B low halogen requirements of <=1000ppm threshold. Antimony trioxide based flame retardants must also meet the <=1000ppm threshold requirement.

(3) MSL, Peak Temp. - The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.

(4) There may be additional marking, which relates to the logo, the lot trace code information, or the environmental category on the device.

(5) Multiple Device Markings will be inside parentheses. Only one Device Marking contained in parentheses and separated by a "~" will appear on a device. If a line is indented then it is a continuation of the previous line and the two combined represent the entire Device Marking for that device.

(6) Lead finish/Ball material - Orderable Devices may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead finish/Ball material values may wrap to two lines if the finish value exceeds the maximum column width.

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PACKAGE OPTION ADDENDUM

TEXAS

TAPE AND REEL INFORMATION

ISTRUMENTS

QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE

Pack Materials-Page 1

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PACKAGE MATERIALS INFORMATION

*All dimensions are nominal

GENERIC PACKAGE VIEW

PWP 14 PWP 14 POWERPAD TSSOP - 1.2 mm max height

4.4 x 5.0, 0.65 mm pitch PLASTIC SMALL OUTLINE

This image is a representation of the package family, actual package may vary. Refer to the product data sheet for package details.

PACKAGE OUTLINE

PWP0014K PowerPAD TSSOP - 1.2 mm max height TM

SMALL OUTLINE PACKAGE

NOTES:

PowerPAD is a trademark of Texas Instruments.

- 1. All linear dimensions are in millimeters. Any dimensions in parenthesis are for reference only. Dimensioning and tolerancing per ASME Y14.5M.
- 2. This drawing is subject to change without notice.
- 3. This dimension does not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not exceed 0.15 mm per side.
- 4. Reference JEDEC registration MO-153.
- 5. Features may differ or may not be present.

EXAMPLE BOARD LAYOUT

PWP0014K PowerPAD TSSOP - 1.2 mm max height TM

SMALL OUTLINE PACKAGE

NOTES: (continued)

- 6. Publication IPC-7351 may have alternate designs.
- 7. Solder mask tolerances between and around signal pads can vary based on board fabrication site.
- 8. This package is designed to be soldered to a thermal pad on the board. For more information, see Texas Instruments literature numbers SLMA002 (www.ti.com/lit/slma002) and SLMA004 (www.ti.com/lit/slma004).
- 9. Size of metal pad may vary due to creepage requirement.
- 10. Vias are optional depending on application, refer to device data sheet. It is recommended that vias under paste be filled, plugged or tented.

EXAMPLE STENCIL DESIGN

PWP0014K PowerPAD TSSOP - 1.2 mm max height TM

SMALL OUTLINE PACKAGE

NOTES: (continued)

11. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.

12. Board assembly site may have different recommendations for stencil design.

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