

**I/Q Modulator/Demodulator and Synthesizer**



The HFA3783 is a highly integrated and fully differential SiGe baseband converter for half duplex wireless applications. It features all the necessary blocks for quadrature

modulation and demodulation of "I" and "Q" baseband signals.

It has an integrated AGC receive IF amplifier with frequency response to 600MHz. The AGC has 70dB of voltage gain and better than 70dB of gain control range. The transmit output also features gain control with 70dB of range.

The receive and transmit IF paths can share a common differential matching network to reduce the filter component count required for single IF half duplex transceivers. A pair of 2nd order antialiasing filters with an integrated DC offset cancellation architecture is included in the receive chain for baseband operation down to DC. In addition, an IF level detector is included in the AGC chain for threshold comparison. Up and down conversion are performed by doubly balanced mixers for "I" and "Q" IF processing. These converters are driven by a broadband quadrature LO generator with frequency of operation phase locked by an internal 3 wire interface synthesizer and PLL.

The device operates at low LO levels from an external VCO with a PLL reference signal up to 50MHz. The HFA3783 is housed in a thin 48 lead LQFP package well suited for PCMCIA board applications.

**Features**

- Integrates All IF Transmit and Receive Functions
- Broad Quadrature Frequency Range . . . . .70 to 600MHz
- 600MHz AGC IF Strip with Level Detector . . . . .69dB
- DC Coupled Baseband Interfaces
- Integrates a Receiver DC Offset Calibration Loop
- Integrated 3 Wire Interface PLL For LO Applications
- Low LO Drive Level . . . . . -15dBm
- Fast Transmit-Receive Switching . . . . . <1μs
- Power Management/Standby Mode
- Single Supply 2.7 to 3.3V Operation

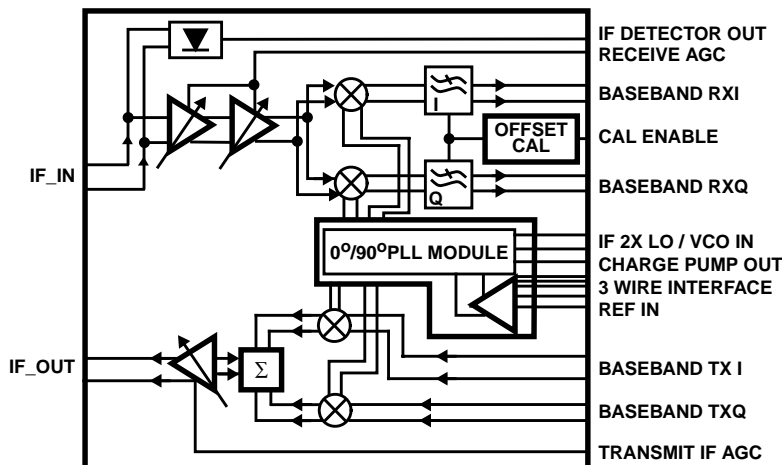
**Applications**

- IEEE802.11 1 and 2Mbps Standard
- Systems Targeting IEEE 802.11 11Mbps Standard
- Wireless Local Area Networks
- PCMCIA Wireless Transceivers
- ISM Systems
- TDMA Packet Protocol Radios

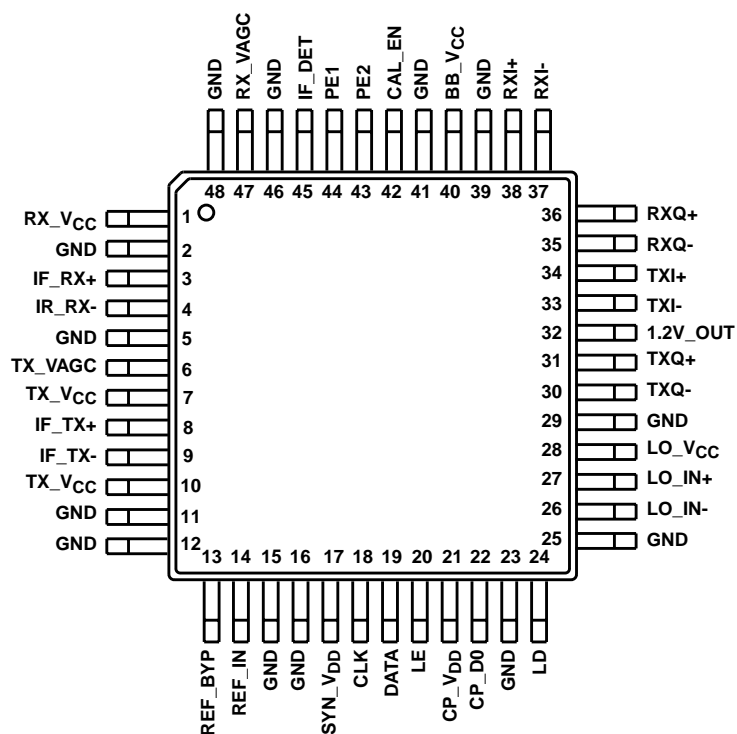
**Ordering Information**

PART NUMBER	TEMP. RANGE (°C)	PACKAGE	PKG. NO.
HFA3783IN	-40 to 85	48 Ld LQFP	Q48.7x7A
HFA3783IN96	-40 to 85	Tape and Reel	

**Simplified Block Diagram**



Pinout



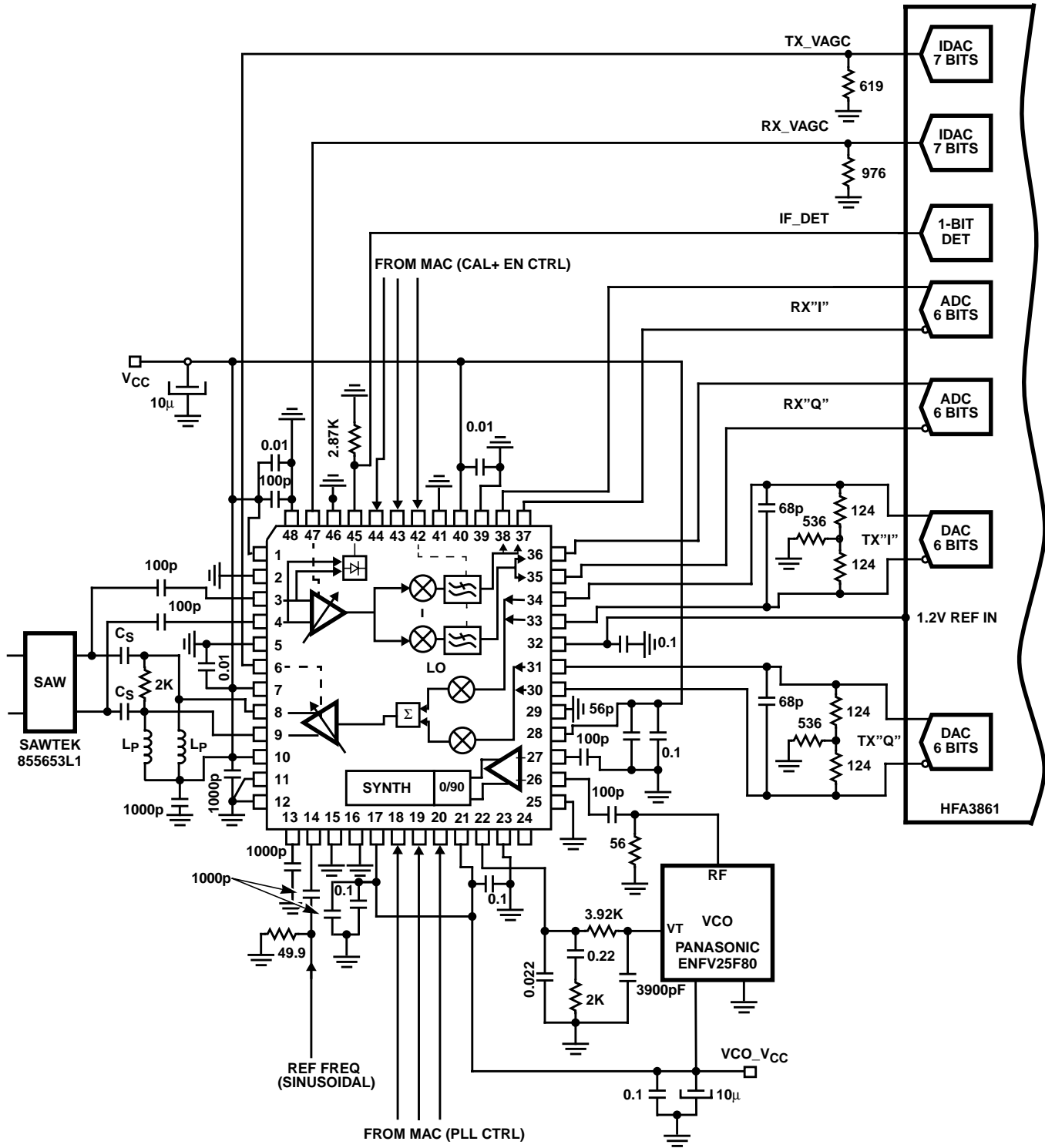
Pin Descriptions

PIN NUMBER	NAME	DESCRIPTION
1	RX_VCC	Receive AGC Amplifier Power Supply. Requires high quality capacitor decoupling.
3	IF_RX+	Receive AGC Differential Amplifier Non-Inverting IF Input. Requires a DC blocking capacitor.
4	IF_RX-	Receive AGC Differential Amplifier Inverting IF Input. Requires a DC blocking capacitor. Pins 3 and 4 are interchangeable and can be used single ended with the other being capacitively bypassed to ground.
6	TX_VAGC	Transmit AGC amplifier DC gain control input.
7	TX_VCC	Transmit AGC Amplifier Power Supply. Requires high quality capacitor decoupling.
8	IF_TX+	Transmit AGC Differential Amplifier Positive Output. Open collector requiring DC bias from V <sub>CC</sub> through an inductor.
9	IF_TX-	Transmit AGC Differential Amplifier Negative Output. Open collector requiring DC bias from V <sub>CC</sub> through an inductor.
10	TX_VCC	Transmit AGC Amplifier Power Supply. Requires high quality capacitor decoupling.
13	REF_BYP	PLL Reference Buffer Signal Negative Differential Input. Pin has active bias and can be used in conjunction with pin 14 either differential or single ended. CMOS inputs must be DC coupled. Small sinusoidal inputs must be DC blocked with this pin bypassed to ground via a capacitor.
14	REF_IN	PLL Reference Buffer Signal Positive Differential Input. Pin has active bias and can be used in conjunction with pin 13 either differential or single ended. CMOS inputs must be DC coupled. Small sinusoidal inputs must be DC blocked with this pin used as an input for the reference signal. When used with single ended CMOS inputs, pin 13 must be left floating. Pins 13 and 14 are interchangeable.
17	SYN_VDD	PLL Synthesizer Digital Power Supply. Requires high quality capacitor decoupling.
18	CLK	PLL Synthesizer Serial Interface Clock. CMOS input.
19	DATA	PLL Synthesizer Serial Interface Data. CMOS input.
20	LE	PLL Synthesizer Serial Interface Latch Enable Control. CMOS input.

**Pin Descriptions** (Continued)

PIN NUMBER	NAME	DESCRIPTION
21	CP_VDD	PLL Charge Pump Power Supply. Independent supply for the charge pump, not to exceed 3.6V. Requires high quality capacitor decoupling.
22	CP_D0	PLL Charge Pump Current Output.
24	LD	PLL Lock Detect Output. Requires low capacitive loading not to exceed 5pF.
26	LO_IN-	Local Oscillator Differential Buffer Negative Input. Requires AC coupling. For single ended applications its complementary input, Pin 27, must be bypassed to ground via a capacitor.
27	LO_IN+	Local Oscillator Differential Buffer Positive Input. Requires AC coupling. For single ended applications its complementary input, Pin 26, must be bypassed to ground via a capacitor. Pins 26 and 27 are interchangeable. NOTE: High second harmonic content LO waveforms may degrade I/Q phase accuracy.
28	LO_VCC	Local Oscillator Buffer Amplifier Power Supply. Requires high quality capacitor decoupling.
30	TXQ-	Baseband Quadrature Differential Inputs for IF Transmission. DC coupled requiring 1.3V common mode bias voltages.
31	TXQ+	
32	1.2V_OUT	Highly Regulated Band Gap 1.2V Buffered Output. Used in conjunction with ADCs and DACs for voltage /temperature tracking. Requires high quality 0.1 $\mu$ F capacitor decoupling to ground.
33	TXI-	Baseband In Phase Differential Inputs for IF Transmission. DC coupled requiring 1.3V common mode bias voltages.
34	TXI+	
35	RXQ-	Baseband Quadrature Differential Outputs From IF Demodulation. DC coupled output with 1.2V common mode DC outputs. AC coupling pins 35, 36, 37 and 38 requires programmable register activation for DC hold during TX to RX switching.
36	RXQ+	
37	RXI-	Baseband In Phase Differential Outputs From IF Demodulation. DC coupled output with 1.2V common mode DC outputs.
38	RXI+	
40	BB_VCC	Baseband Receive LPF Output and Offset Control Power Supply. Requires high quality capacitor decoupling.
42	CAL_EN	CMOS Input for Activation Of Internal DC Offset Adjust Circuit for the Receive Baseband Outputs. A rising edge activates the calibration cycle, which completes within a programmable time and holds the calibration while this pin is held high. In applications where the synthesizer is not used, this pin needs to be grounded.
43	PE2	Power Enable Control Pins: Please refer to the POWER ENABLE TRUTH TABLE in the Electrical Specifications section.
44	PE1	
45	IF_DET	IF Detector Current Output. A current source of 175 $\mu$ A typical is generated at this pin when the IF AGC receive differential or single ended signal at pins 3 and 4 is between 100 and 200mV <sub>pp</sub> .
47	RX_VAGC	Receive AGC amplifier DC gain control input.
2, 5, 11, 12, 15, 16, 23, 25, 29, 39, 41, 46, 48	GND	Grounds. Connect to a solid ground plane.

Application Circuit







## HFA3783

### Receive Cascaded AC Electrical Specification IF = 375MHz, LO = 748MHz, V<sub>CC</sub> = 2.7V, Unless Otherwise Specified (Continued)

PARAMETER	TEST CONDITIONS	TEMP. (°C)	MIN	TYP	MAX	UNITS
Voltage Gain	AGC Control Voltage set to 10dB attenuation. Differential 250Ω input, differential 5kΩ output load.	Full	-	59	-	dB
Power Gain		Full	-	46	-	dB
Cascaded Noise Figure		Full	-	-	11	dB
Output IP3		Full	+1.5	-	-	dBm
Output P1dB		Full	-14.3	-	-	dBm
Voltage Gain	AGC Control Voltage set to 20dB attenuation. Differential 250Ω input, differential 5kΩ output load.	Full	-	49	-	dB
Power Gain		Full	-	36	-	dB
Cascaded Noise Figure		Full	-	14.1	-	dB
Output IP3		Full	+1.0	-	-	dBm
Output P1dB		Full	-14.4	-	-	dBm
Voltage Gain	AGC Control Voltage set to 30dB attenuation. Differential 250Ω input, differential 5kΩ output load.	Full	-	39	-	dB
Power Gain		Full	-	26	-	dB
Cascaded Noise Figure		Full	-	19.9	-	dB
Output IP3		Full	+0.3	-	-	dBm
Output P1dB		Full	-14.6	-	-	dBm
Voltage Gain	AGC Control Voltage set to 40dB attenuation. Differential 250Ω input, differential 5kΩ output load.	Full	-	29	-	dB
Power Gain		Full	-	16	-	dB
Cascaded Noise Figure		Full	-	27	-	dB
Output IP3		Full	-1.4	.74	2.8	dBm
Output P1dB		Full	-15.0	-	-	dBm
Voltage Gain	AGC Control Voltage set to 50dB attenuation. Differential 250Ω input, differential 5kΩ output load.	Full	-	19	-	dB
Power Gain		Full	-	6	-	dB
Cascaded Noise Figure		Full	-	35.1	-	dB
Output IP3		0-85	-2.0	-	-	dBm
Output P1dB		0-85	-15.5	-	-	dBm
Voltage Gain	AGC Control Voltage set to 60dB attenuation. Differential 250Ω input, differential 5kΩ output load.	Full	-	9	-	dB
Power Gain		Full	-	-4	-	dB
Cascaded Noise Figure		Full	-	43.9	-	dB
Output IP3		0-85	-3.3	-	-	dBm
Output P1dB		0-85	-16.1	-	-	dBm
Voltage Gain	AGC Control Voltage set to 72dB attenuation. Differential 250Ω input, differential 5kΩ output load.	Full	-	-3	-	dB
Power Gain		Full	-	-16	-	dB
Cascaded Noise Figure		Full	-	60.0	-	dB
Output IP3		0-85	-6.7	-	-	dBm
Output P1dB		0-85	-18.2	-	-	dBm
Minimum Power Gain	V <sub>AGC</sub> = 2.25V	25	-	-	-17	dB
AGC Gain Control Voltage		Full	0.2	-	2.25	V
AGC Gain Control Sensitivity	Over Supply Range	Full	-	61.6	-	dB/V

## HFA3783

### Receive Cascaded AC Electrical Specification IF = 375MHz, LO = 748MHz, V<sub>CC</sub> = 2.7V, Unless Otherwise Specified (Continued)

PARAMETER	TEST CONDITIONS	TEMP. (°C)	MIN	TYP	MAX	UNITS
AGC Gain Control Input Impedance		Full	20	23	-	kΩ
Gain Switching Speed to ±1dB Settling	Full AGC Scale	Full	-	0.4	1	μs
Insertion Phase vs AGC	Full AGC Range	25	-2	±0.3	+2	deg/dB
IF Detector Response Time	10pF, 2.9K External Load	Full	-	0.15	0.25	μs
IF Detector Input Voltage	0.5V, 175μA Into 2.87K Out	Full	100	150	200	mV <sub>PP</sub>
LO Internal Input Resistance	Single End. 748MHz	25	950	-	1.1K	Ω
LO Internal Input Capacitance		25	-	0.96	-	pF
LO Drive Level	External 50Ω Match Network (single resistor)	Full	-15	-10	0	dBm
Upper Baseband 3dB Bandwidth (2nd Order)		Full	6.7	7.4	8.5	MHz
Lower Baseband 3dB Bandwidth	DC Coupled Load	Full	DC	-	-	-
I and Q 3dB BW Matching		Full	-2	-	+2	%
Cascaded Receive I or Q Baseband THD	1MHz, 1V <sub>PP</sub> Diff. for First 50dB of Attenuation Range	25	-	-	1	%
Cascaded Receive I/Q Crosstalk		25	-	-	-40	dB
I/Q Amplitude Balance	100kHz CW	Full	-1	-	+1	dB
I/Q Phase Balance	100kHz CW	Full	-2	-	+2	deg
Cascaded I or Q Baseband Differential Offset Voltage	After Calibration Cycle. Measured with a setting of 26dB of power gain	Full	-	-	10	mV
Cascaded I or Q Common Mode Voltage at Baseband		Full	1.08	1.17	1.32	V
Offset Calibration Time	Ref = 44MHz, Offset Counter C = 25	Full	-	25	-	μs
Offset Counter Divide Ratio (C Counter)	Input Ref Clock is Divided by C- 2 for SAR Offset Correction	Full	1	-	127	-
CAL_EN Minimum Pulse Width	High to Low to High Transition Time	Full	0	-	-	nS
Baseband Output Resistance Loading	Differential. 1/2 value for ground reference loads	Full	-	5	-	kΩ
Baseband Output Capacitance Loading	Single End, Each	Full	-	-	10	pF
	Differential	Full	-	-	10	pF

**NOTE:**

- A positive frequency offset from the carrier produces I leading Q by 90 degrees.

### Transmit Cascaded AC Electrical Specifications LO = 748MHz, V<sub>CC</sub> = 2.7V, V<sub>CM</sub> = 1.24V Unless Otherwise Specified

PARAMETER	TEST CONDITIONS	TEMP. (°C)	MIN	TYP	MAX	UNITS
IF Frequency Range	Test Diagram	Full	70	-	600	MHz
2 X LO Frequency Range	Test Diagram	Full	140	-	1200	MHz
Output Power at 250Ω Differential Load	AGC Voltage Set to -10dBm Output Power for 0.35V <sub>PP</sub> Sine I and Q Inputs	Full	-	-10	-	dBm
Output Noise Floor		Full	-	-141	-	dBm/Hz
P1dB/Output Power Ratio		Full	10	-	-	dB



## HFA3783

### Transmit Cascaded AC Electrical Specifications LO = 748MHz, V<sub>CC</sub> = 2.7V, V<sub>CM</sub> = 1.24V Unless Otherwise Specified (Continued)

PARAMETER	TEST CONDITIONS	TEMP. (°C)	MIN	TYP	MAX	UNITS
Output Power at 250Ω Differential Load	AGC Voltage Set to 10dB Attenuation. 0.35V <sub>PP</sub> Sine I and Q Inputs	Full	-	-20	-	dBm
Output Noise Floor		Full	-	-149	-	dBm/Hz
P1dB/Output Power Ratio		Full	10	-	-	dB
Output Power at 250Ω Differential Load	AGC Voltage Set to 20dB Attenuation. 0.35V <sub>PP</sub> Sine I and Q Inputs	Full	-	-30	-	dBm
Output Noise Floor		Full	-	-157	-	dBm/Hz
P1dB/Output Power Ratio		Full	10	-	-	dB
Output Power at 250Ω Differential Load	AGC Voltage Set to 30dB Attenuation. 0.35V <sub>PP</sub> Sine I and Q Inputs	Full	-	-40	-	dBm
Output Noise Floor		Full	-	-161	-	dBm/Hz
P1dB/Output Power Ratio		Full	10	-	-	dB
Output Power at 250Ω Differential Load	AGC Voltage Set to 40dB Attenuation. 0.35V <sub>PP</sub> Sine I and Q Inputs	Full	-	-50	-	dBm
Output Noise Floor		Full	-	-162	-	dBm/Hz
P1dB/Output Power Ratio		Full	10	-	-	dB
Output Power at 250Ω Differential Load	AGC Voltage Set to 50dB Attenuation. 0.35V <sub>PP</sub> Sine I and Q Inputs	Full	-	-60	-	dBm
Output Noise Floor		Full	-	-163	-	dBm/Hz
P1dB/Output Power Ratio		Full	10	-	-	dB
Output Power at 250Ω Differential Load	AGC Voltage Set to 60dB Attenuation. 0.35V <sub>PP</sub> Sine I and Q Inputs	Full	-	-70	-	dBm
Output Noise Floor		Full	-	-164	-	dBm/Hz
P1dB/Output Power Ratio		Full	10	-	-	dB
Output Power at 250Ω Differential Load	AGC Voltage Set to 70dB Attenuation. 0.35V <sub>PP</sub> Sine I and Q Inputs	Full	-	-80	-	dBm
Output Noise Floor		Full	-	-164	-	dBm/Hz
P1dB/Output Power Ratio		Full	10	-	-	dB
AGC Gain Control Voltage		Full	0.1	-	2.25	V
AGC Gain Control Sensitivity	Supply Range	25	-	35.4	-	dB/V
AGC Control Input Impedance		Full	20	21	-	kΩ
Gain Switching Speed to ±1% Settling	Full Scale	25	-	0.8	4	μs
Insertion Phase vs AGC	50dB Range from Max	Full	-	-	4.0	deg
I/Q Baseband Bandwidth	Application Circuit	Full	0	13	-	MHz
Cascaded Baseband to IF TX THD	1MHz, 0.5V <sub>PP</sub>	25	-	-	0.5	%
Amplitude Balance	DC Inputs	25	-0.5	-	+0.5	dB
Phase Balance	DC Inputs	25	-2	-	+2	deg
Carrier Suppression	Full AGC Range	25	-	-43	-30	dBc
SSB Sideband Suppression (Note 5)	100kHz Inputs, Full AGC Range	25	-	-43	-32	dBc
Optimum IF Output Differential Impedance	Shared with RX	25	-	250	-	Ω
LO Internal Input Resistance	Single End Across F. Range Same as RX Section	25	950	-	1.1K	Ω
LO Internal Input Capacitance		25	-	0.96	-	pF
LO Drive Level	External 50Ω Match Network (single resistor)	Full	-15	-10	0	dBm
Baseband Differential Input Impedance		Full	100	150	-	kΩ
Optimum Baseband Differential Input Voltage	Shaped Pulses	Full	-	0.5	-	V <sub>PP</sub>
Common Mode Baseband Input Voltage Range	All TX Inputs	Full	1.2	1.30	1.40	V

NOTE:

5. I leading Q produces a+jw CCW rotation and a positive frequency offset from the carrier.

**Phase Lock Loop Electrical Specifications**

PARAMETER	TEST CONDITIONS	TEMP. (°C)	MIN	TYP	MAX	UNITS
Operating 2X LO Frequency	Test Diagram	Full	140	-	1200	MHz
Reference Oscillator Frequency	Test Diagram	Full	-	-	50	MHz
Selectable Prescaler Ratios (2 Settings)		Full	16/17	N/A	32/33	-
Swallow Counter Divide Ratio (A Counter)		Full	0	-	127	-
Programmable Counter Divide Ratio (B Counter)		Full	3	-	2047	-
Reference Counter Divide Ratio (R Counter)		Full	3	-	32767	-
Reference Oscillator Sensitivity	Single or Differential Sine Inputs	Full	0.5	-	-	V <sub>PP</sub>
	CMOS Single or Complementary	Full	-	CMOS	-	-
Reference Oscillator Duty Cycle	CMOS Inputs	Full	40	-	60	%
Charge Pump Sink/Source Current/Tolerance	250µA Selection +/- 25%	Full	0.18	0.25	0.32	mA
Charge Pump Sink/Source Current/Tolerance	500µA Selection +/- 25%	Full	0.375	0.5	0.625	mA
Charge Pump Sink/Source Current/Tolerance	750µA Selection +/- 25%	Full	0.56	0.75	0.94	mA
Charge Pump Sink/Source Current/Tolerance	1mA Selection +/- 25%	Full	0.75	1.0	1.25	mA
Charge Pump Sink/Source Mismatch		Full	-	-	15	%
Charge Pump Output Compliance		Full	0.5	-	CPV <sub>DD</sub> -0.5	V
Charge Pump High Z leakage	High Z state	Full	-10	±0.1	10	µA
Charge Pump Supply Voltage		Full	2.7	-	3.6	V
Serial Interface Clock Width	High Level	Full	20	-	-	ns
	Low level	Full	20	-	-	ns
Serial Interface Data/Clk Set-Up Time		Full	20	-	-	ns
Serial Interface Data/Clk Hold Time		Full	10	-	-	ns
Serial Interface Clk/LE Set-Up Time		Full	20	-	-	ns
Serial Interface LE Pulse Width		Full	20	-	-	ns

**POWER ENABLE TRUTH TABLE**

PE1	PE2	PLL_PE (SERIAL BUS)	STATUS
0	0	1	Power Down State, PLL Registers in Save Mode, Inactive PLL, Active Serial Interface
1	1	1	Receive State, Active PLL
1	0	1	Transmit State, Active PLL
0	1	1	Inactive Transmit and Receive States, Active PLL, Active Serial Interface
X	X	0	Inactive PLL, Disabled PLL Registers, Active Serial Interface

**PLL Synthesizer and DC Offset Clock Programming Table**

SERIAL BITS	REGISTER DEFINITION																				
	LSB 1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	MSB	
R Counter	0	0	R(0)	R(1)	R(2)	R(3)	R(4)	R(5)	R(6)	R(7)	R(8)	R(9)	R(10)	R(11)	R(12)	R(13)	R(14)	X (Don't Care)			
A/B Counter	0	1	A(0)	A(1)	A(2)	A(3)	A(4)	A(5)	A(6)	B(0)	B(1)	B(2)	B(3)	B(4)	B(5)	B(6)	B(7)	B(8)	B(9)	B(10)	

**PLL Synthesizer and DC Offset Clock Programming Table (Continued)**

SERIAL BITS	REGISTER DEFINITION																			
	LSB 1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	MSB
Operational Mode	1	0	M(0)	0	M(2)	M(3)	M(4)	M(5)	M(6)	M(7)	M(8)	0	0	0	0	M(13)	M(14)	M(15)	X	X
Offset Calibration	1	1	C(0)	C(1)	C(2)	C(3)	C(4)	C(5)	C(6)	0	0	0	0	C(11)	X (Don't Care)					

NOTES:

- The Serial data is clocked on the Rising Edge of the serial clock, MSB first. The serial Interface is active when LE is LOW. The serial Data is latched into defined registers on the rising edge of LE.
- The M register or Operational Mode needs to be loaded first. Registers R, A/B and Offset Calibration follow M loading in any sequence.

**Reference Frequency Counter/Divider**

BIT	DESCRIPTION
R(0-14)	Least significant bit R(0) to most significant bit R(14) of the divide by R counter. The Reference signal frequency is divided down by this counter and is compared with a divided LO by a phase detector.

**LO Frequency Counters/Dividers**

BIT	DESCRIPTION
A(0-6)	Least significant bit A(0) to most significant bit A(6) of a 7-bit Swallow counter and LSB B(0) to MSB B(10) of the 11 bits divider. The LO frequency is divided down by [P*B+A], where P is the prescaler divider set by bit M(2). This divided signal frequency is compared by a phase detector with the divided Reference signal.
B(0-10)	

**Operational Modes**

BIT	DESCRIPTION				
M(0)	(PLL_PE), Phase Lock Loop Power Enable. 1 = Enable, 0 = Power Down. Serial port always on.				
M(2)	Prescaler Select. <b>0 = 16/17, 1 = 32/33</b>				
M(3) M(4)	Charge Pump Current Setting.	<b>M(4)</b>	<b>M(3)</b>	<b>OUTPUT SINK/SOURCE</b>	
		0	0	0.25mA	
		0	1	0.50mA	
		1	0	0.75mA	
		1	1	1.00mA	
M(5) M(6)	Charge Pump Sign.	<b>M(6)</b>	<b>M(5)</b>		
		0	0	Source Current if LO/ [P*B+A] < Ref/R	
		0	1	Source Current if LO/ [P*B+A] > Ref/R	
M(7) M(8) M(13)	LD Pin Multiplex Operation.	<b>M(13)</b>	<b>M(8)</b>	<b>M(7)</b>	<b>OUTPUT AT PIN LD</b>
		0	0	X	Lock Detect Operation
		0	1	X	Short to GND
		1	0	X	Serial Register Read Back
		1	1	0	Ref. Divided by R Waveform
		1	1	1	LO Divided by [P*B+A] Waveform
M(14) M(15)	Charge Pump Operation/Test.	<b>M(15)</b>	<b>M(14)</b>	<b>OPERATION/TEST</b>	
		0	0	Normal Operation	
		0	1	Charge Pump Constant Current Source	
		1	0	Charge Pump Constant Current Sink	
		1	1	High Impedance State	

DC Offset Calibration Counter

BIT	DESCRIPTION
C(0-6)	Least Significant bit C(0) to Most significant bit C(6) of the offset calibration counter/divider. The calibration clock frequency and calibration time is defined by the Reference signal frequency divided down by this counter as follows: $\text{CAL TIME} = 22 * \frac{2 * C}{\text{REFIN (MHz)}}$
C(11)	Set output bias level for AC coupling applications and TX/RX switching improvement in performance.

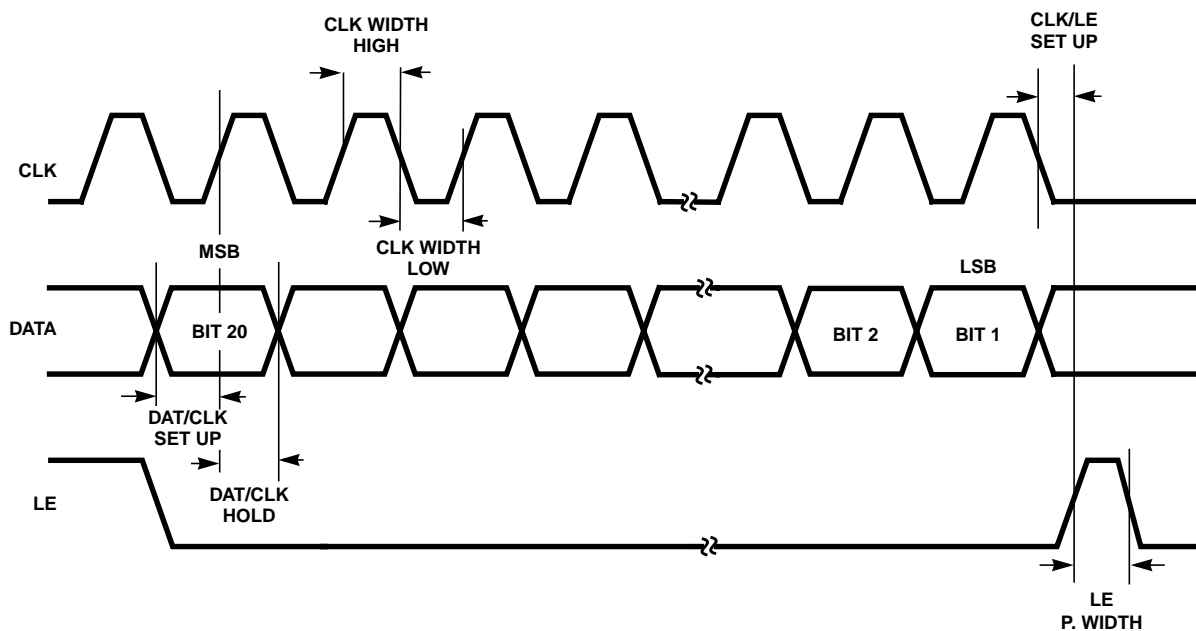


FIGURE 1. PLL SYNTHESIZER SERIAL INTERFACE TIMING DIAGRAM

**S Parameter Tables****RX DIFFERENTIAL INPUT, LINEAR MODE**

FREQ (MHz)	MAG	ANGLE
70	0.886	-2.6
140	0.886	-4.7
200	0.886	-6.6
280	0.885	-9.4
380	0.885	-12.8
500	0.883	-16.9
600	0.883	-20.1

**TX DIFF OUT AT RX-MODE**

FREQ (MHz)	MAG	ANGLE
70	1	-1.0
140	1	-1.9
200	1	-2.8
280	1	-3.9
380	1	-5.2
500	0.999	-6.8
600	0.999	-8.0

**RX DIFFERENTIAL INPUT, TX MODE**

FREQ (MHz)	MAG	ANGLE
70	0.877	-4.4
140	0.873	-7.4
200	0.870	-10.5
280	0.866	-14.5
380	0.862	-19.6
500	0.857	-25.7
600	0.853	-30.5

**LO INPUT SINGLE END**

FREQ (MHz)	MAG	ANGLE
140	0.923	-5.1
400	0.920	-13.4
560	0.917	-19.0
760	0.911	-25.9
1000	0.900	-34.8
1200	0.890	-42.3

**RX DIFFERENTIAL INPUT, SATURATED**

FREQ (MHz)	MAG	ANGLE
70	0.883	-2.5
140	0.881	-5.7
200	0.878	-8.4
280	0.875	-11.9
380	0.869	-16.2
500	0.859	-21.3
600	0.850	-25.4

**REF IN SINGLE END**

FREQ (MHz)	RESISTOR /CAPACITANCE PARALLEL	
10	5.8K	0.840p
30	5.7K	0.850p
50	5.7K	0.860p

**RX SINGLE END IN LINEAR MODE**

FREQ (MHz)	MAG	ANGLE
70	0.873	-4.0
140	0.872	-7.1
200	0.870	-10.1
280	0.869	-14.2
380	0.870	-19.3
500	0.872	-25.6
600	0.872	-30.8

**TX DIFFERENTIAL OUTPUT**

FREQ (MHz)	MAG	ANGLE
70	1	-1.1
140	1	-2.0
200	0.999	-2.8
280	0.999	-3.9
380	0.999	-5.4
500	0.999	-7.1
600	0.997	-8.3

## Overall Device Description

The HFA3783 is a highly integrated baseband converter for half duplex wireless data applications. It features all the necessary blocks for baseband modulation and demodulation of “I” and “Q” quadrature multiplexing signals including an on chip three wire interface PLL stage used with an external VCO for Local Oscillator applications. Device RF properties have been optimized through the thoughtful consideration of layout, device pinout, and a completely differential design. These RF properties include immunity from common mode signals such as noise and crosstalk, optimized dynamic range for low power requirements and reduced relevant parasitics and settling times. The single power supply requirements from  $2.7V_{DC}$  to  $3.3V_{DC}$  makes the HFA3783 a good choice for portable transceiver designs.

### Receive Chain

The HFA3783 has two cascaded very low distortion integrated AGC IF amplifiers with frequency response from 70 to 600MHz. These differential amplifiers exhibit better than 70dB of both voltage gain and AGC range. Noise figure, output compression and intercept point variations with the AGC range have been tailored to achieve cascaded performances as presented in the AC Electrical Specifications. To increase the receiver’s overall AGC dynamic range and conserve compression specifications, a Peak Detector has been added in parallel with the AGC’s input. The Peak Detector is used to control an external step attenuator or the RF gain of the front end LNA stage. Following the AGC stages, an AC coupled down conversion pair of quadrature doubly balanced mixers are used for “I” and “Q” baseband IF processing. These differential converters are driven by an internal differential quadrature generator with broadband response and excellent quadrature properties. For broadband operation, the Local Oscillator frequency input is twice the desired frequency of demodulation. Duty cycle and signal purity requirements for the 2XLO input using this type of quadrature architecture are less restrictive for the HFA3783. Ground reference or differential input signals from -15dBm to 0dBm and frequencies up to 1200MHz (2XLO) can be used.

The output of the “I” and “Q” mixers are DC coupled to a pair of multistage differential 2nd pole antialiasing baseband filters with DC offset correction. The DC offset correction is enabled with an external control pin allowing for correction to occur during transmit, receive or power down modes. The baseband filter’s cut off frequency of 7.7MHz is optimized for 11M chips/s spread spectrum applications. The baseband outputs are differential, with common mode DC voltage outputs tracking an internal band gap voltage reference. The Band Gap reference is also available to the user by an external pin. The “I” and “Q” baseband voltages can swing up to 1Vpp differential, following the AC Electrical Specifications across the AGC range. Figure 16 illustrates the cascaded gain characteristics versus AGC voltage control for the HFA3783 receive section.

### Transmit Chain

The HFA3783 modulator section has a frequency response of 70 to 600MHz. It consists of differential “I” and “Q” baseband inputs requiring pre-shaped analog data levels up to 500mVpp. A common mode voltage of around 1.3V is required for proper operation of the four differential input pins. There are no internal pre-shaping filters in the modulator section. Following the differential input stages, a DC coupled up conversion pair of quadrature doubly balanced mixers are used for “I” and “Q” baseband IF processing. These differential mixers are driven by the same internal LO quadrature generator used in the receive section. Their phase and gain characteristics, including I/Q matching, are well suitable for accurate data transmission. The final stage is an AGC amplifier with 70dB of dynamic range. Please refer to Figure 35.

## Detailed Description

### Receive AGC/ Peak Detector

The receive AGC amplifier section consists of 4 stages and each stage is built out of four parallel, distributed gain/degeneration differential pairs. In half duplex packet transmission linear systems, the receive AGC control’s thermal and supply voltage variations over the packet duration are more important than gain control linearity. Therefore, the chosen architecture addresses very constricted temperature, voltage and process variations. The control is based on a band gap voltage reference “gm” distribution scheme. In addition, the design provides fast AGC settling times as well as fast turn on/off characteristics for packetized information. The four stage AGC amplifier has a typical maximum voltage gain of 44dB and exhibits better than 70dB of dynamic range, providing an attenuation in excess of 26dB at minimum gain. The design can be used differential or single ended, exhibiting the same gain characteristics: however, consideration is necessary due to common mode spurious signals. One of the main features of this front end is the high impedance and small variation of S parameters when the HFA3783 is switched between transmit and receive modes. This feature permits the use of a combination match network and the use of a single SAW filter for both halves of the duplex operation. S parameters for the differential and single ended applications are available in the S Parameter Tables of this document. The matching network arrangements will be discussed later in IF Interface section.

A Peak Detector is placed in parallel with the input of the first stage of the AGC amplifier. It consists of a high frequency differential full wave rectifier and a voltage to current converter. The Peak Detector has limited range and is used to trip a comparator in an external baseband processor when the voltage swing at the input of the AGC amplifier is about 150mVpp. Once the external comparator is tripped, its logic output level steps the LNA’s gain down keeping the RF

and IF mixers out of compression. An external resistor and capacitor set both the desired threshold voltage and time constant. Figures 29 and 30 illustrate the typical current output of the Peak Detector for input voltage levels between 100 and 200mVpp.

### **Quadrature Demodulator**

The output of the AGC amplifier is AC coupled to two doubly balanced quadrature differential mixers, for “I” and “Q” demodulation. With full balanced differential architecture, these mixers are driven by an accurate internal Local Oscillator (LO) chain as described later. The voltage gain for both mixers is well matched with a typical value of 8V/V.

### **Low Pass Filter and DC Offset Correction**

To cover baseband signals from DC to 7.7MHz, the outputs of the baseband down converter mixers are DC coupled to the Low Pass Filter stages. For true DC response, the combination of all DC offsets (mixer, LPF and buffers) needs to be calibrated for accurate baseband processing. This calibration can be performed at any time during the receive, transmit or power down modes. Figure 2 depicts the baseband low pass receive filter implementation and Figure 3 shows the calibration internal timing diagram of the HFA3783. Referring to channel “I” for example, calibration begins with the auto balanced comparator measuring the differential offset between the RXI+ and RXI- outputs. The comparator’s output is fed to a decision circuit which changes the condition of a Successive Approximation Register (SAR) state control. The SAR controls 8 bits of a current output Digital to Analog Converter (IDAC) which is divided by weight into a LPF section (2 pole) and a buffer amplifier. The currents are searched and set to bring the offset to a minimum. The LPF has a fixed gain of 2.5V/V and the buffer adds a 1.25V/V final gain to the receive chain.

Referring to Figure 2, clocking to the SAR is provided by a programmable division of the REF\_IN signal. (Used for the PLL as the stable reference.) The frequency of the reference signal is divided down by the register setting of the offset calibration counter. (Details for setting this counter can be found in the Programming the PLL Synthesizer and DC Offset Clock section.)

The output of the calibration counter is again divided by 2 and the period used to generate the time slots of a state sequence. The calibration cycle is initialized by a rising edge on the HFA3783 CAL\_EN pin. The state sequence slots 1 to 7 are used to settle all circuits in case the device is in the power down mode, slots 8 to 10 are used to calibrate the offset comparators (auto balancing) and slots 13 to 21 perform the search with an initial value of approximately + or - 400mV differential DC level. The comparator reads the direction and level of the offset and sets the next level and polarity at + or -400/2 mV. The process continues until slot 21 in a divide by 2 polarity and minimum offset search. The contents of the SAR are kept in slot 22 which holds the IDAC in storage mode until a new positive edge is provided to the CAL\_EN pin. In receive mode, the AGC amplifiers are turned off during the calibration cycle. A typical calibration time from 10 to 25µS is suggested for optimum accuracy.

The baseband outputs of the LPF buffer amplifier drive differential loads of 5KΩ with a common mode voltage of typically 1.17V.

An extra feature of the LPF allows for AC coupling of the baseband differential outputs. To avoid discharging of the AC coupling capacitors between transmit and receive states a common mode voltage can be applied to all outputs. An onboard programmable bit control establishes the application with 4 internal resistors and switches.

### **LO Quadrature Generator**

The In Phase and Quadrature Local oscillator signals are generated by a divide by two circuit that drives both the up and down conversion mixers. With a fully balanced approach, the phase relationship between the two quadrature signals is within  $90^{\circ} \pm 2^{\circ}$  for a wide 70 to 600MHz frequency range. The input signal frequency at the LO\_IN pin needs to be twice the desired Local Oscillator frequency. The high impedance differential LO\_IN+ and LO\_IN- inputs, which are driven by an external VCO, can be used single ended by capacitively bypassing one input to ground. The user needs to terminate the VCO transmission line into the desired impedance and AC couple the active LO\_IN input.

Divide by two LO generation often requires rigid control of signal purity or duty cycles. The HFA3783 has an internal duty cycle compensation circuit which eases the requirements of rigidly controlled duty cycles. Second harmonic contents up to 10% are acceptable.

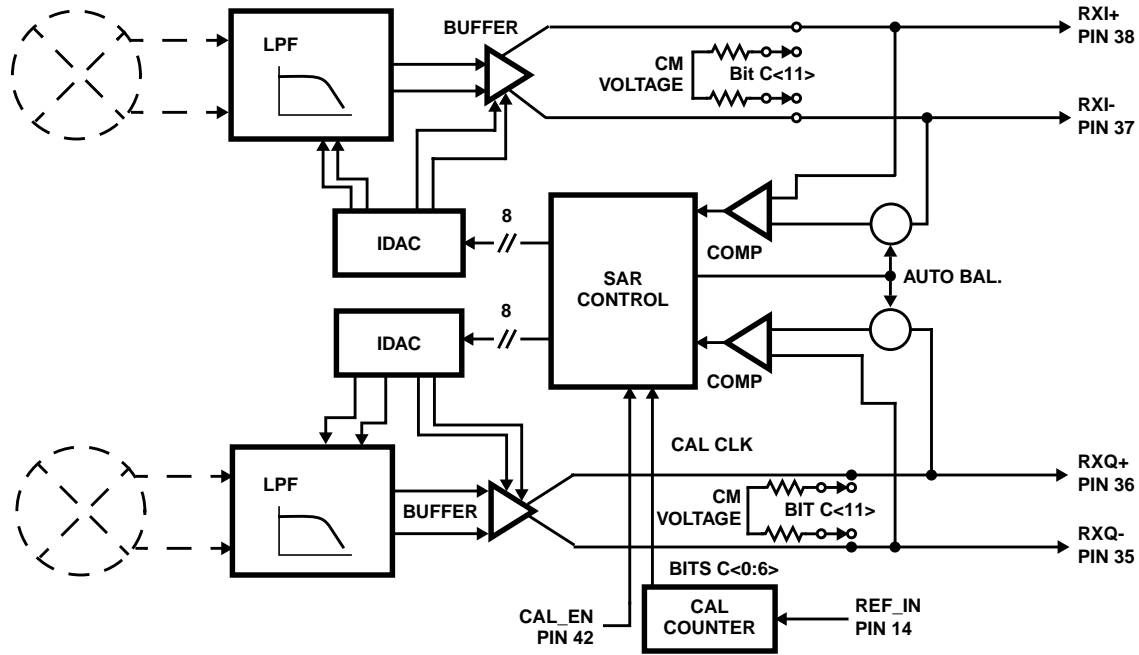


FIGURE 2. DC OFFSET CALIBRATION BLOCK DIAGRAM

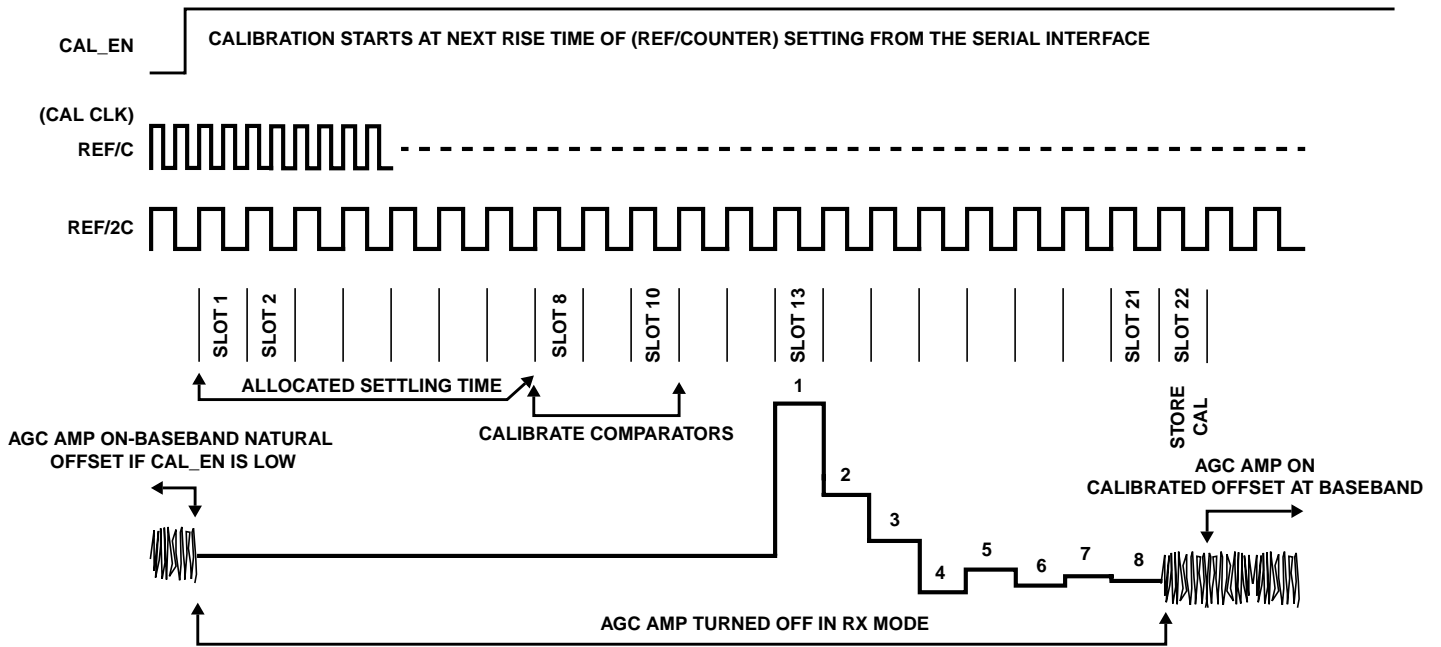


FIGURE 3. DC OFFSET CALIBRATION TIMING DIAGRAM



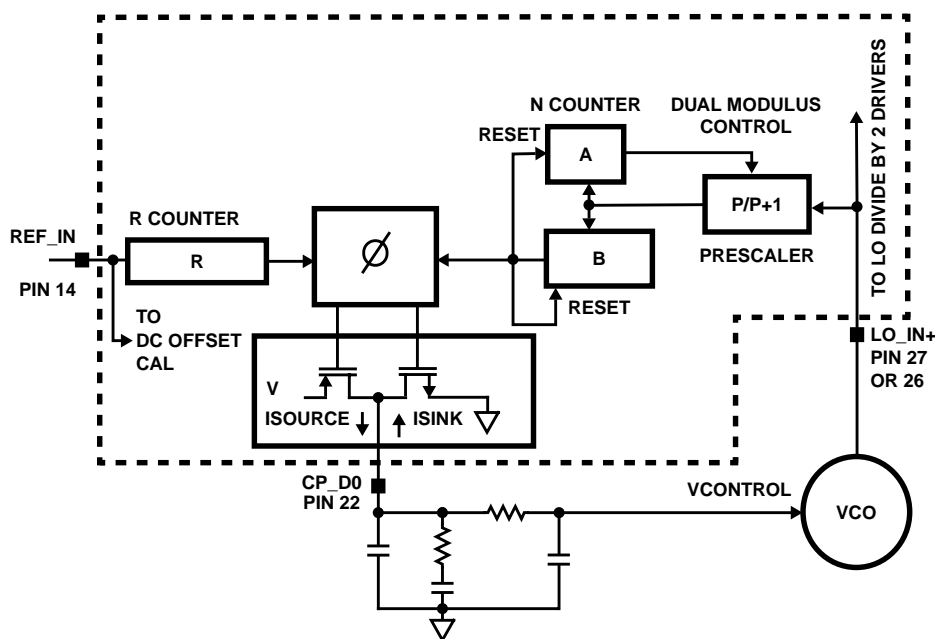


FIGURE 4. PLL SIMPLIFIED BLOCK DIAGRAM

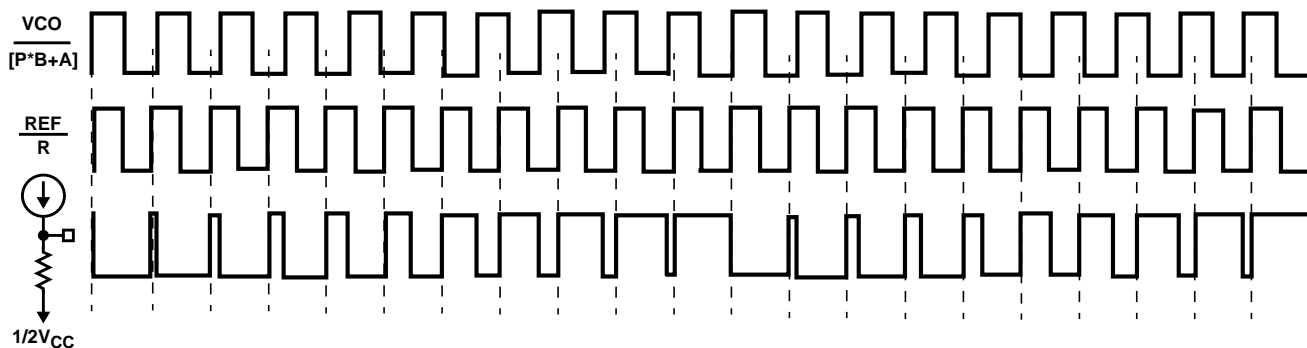


FIGURE 5. CHARGE PUMP OUTPUT FOR TWO SLIGHTLY DIFFERENT FREQUENCY SIGNALS

## PLL

The HFA3783 includes a classical architecture Phase Lock Loop circuit with a three wire serial control interface to be used with an external VCO. Figure 4 depicts a simplified block diagram of the PLL. It consists of a programmable “R” counter used to divide down the frequency of a very stable reference signal up to 50MHz to a phase comparator. A couple of counters (“A” and “B”) with a front end prescaler (“P or P+1”), with dual modulus control, divides down the frequency of an external VCO signal to the same phase comparator. The comparator controls a charge pump circuit and an external loop filter closes the loop for VCO control.

The VCO frequency dividing chain works with a dual modulus control as follows: At the beginning of a count cycle, and if the A counter is programmed with a value greater than zero, the prescaler is set to a division ratio of (P+1) where P can take programmable values of 16 or 32.

Notice that the prescaler output signal is always fed simultaneously to both A and B counters. Upon filling counter A, the prescaler division ratio becomes P and the B counter continues on its own with A in standby. This process is known as “pulse swallowing”. The expression B-A (counts) is the remainder of counts carried out by the B counter after A is full. Both A and B counters are reset at the end of the counting cycle when B fills up. As a result, the total count or division ratio used for the VCO signal is  $A*(P+1) + (B-A)*P$  which simplifies to  $[P*B+A]$ . (A and B counters are referred as the “N” counter).

The Charge Pump (current source/sink) has 4 programmable current settings. This variation allows the user to change the reference frequency for different objectives without changing the loop filter components. The user can program the charge pump sign based on the direction of increase or decrease of the VCO frequency. The

most often used VCO's in the market have positive KVCO's where the VCO frequency increases with an increase in control voltage. In this case, the charge pump current shall "source" current (to the main capacitor of the loop filter) when the VCO frequency becomes less than the desired frequency of operation. The phase comparison and charge pump output behavior in an open loop system is illustrated in Figure 5. The comparator's inputs (the top two waveforms of Figure 5) are from the N and R counters. The output from the "N" counter and the prescaler, labelled as " $VCO/[P*B+A]$ " shows a lower frequency than the output from the "R" counter labeled "REF/R". REF/R is usually called "reference" frequency. The bottom waveform represents the charge pump sourcing current as it has been programmed. Because it is an open loop system, the charge pump current pulse width will increase and follow the phase comparator's output. The charge pump signal can be developed across a resistor connected between pin 22 and a power supply of half the  $V_{CC}$  voltage. In the case where the  $VCO/[P*B+A]$  frequency is higher than the REF/R frequency, the bottom waveform would have negative pulse width variations indicating the Charge Pump sinking current.

The closed loop concept can be understood intuitively by observing the bottom waveform and noticing the tendency of the Charge Pump to "charge" a capacitor (loop filter) and increase the VCO voltage control accordingly. As the  $VCO/[P*B+A]$  frequency becomes higher than the REF/R frequency, the Charge Pump begins to sink current and the VCO control voltage begins to drop. The process would continue in equilibrium with expected sharp reverting polarity

pulses at the REF/R reference frequency. Figure 6 depicts a simple Charge Pump polarity concept and includes the output of the Lock Detect Pin of the HFA3783. This pin has other applications and will be covered in the next section.

### PLL Synthesizer and DC Offset Clock Programming

A three wire CMOS Serial interface (CLK, DATA, LE) programs various counters and operational modes of the HFA3783 PLL. It also programs the DC offset adjust counter and operation of the LPF section. Figure 1 in the Specification section shows the Timing Diagram for this interface.

Short clock periods in the order of 20ns can be used to program this interface. The serial data is clocked on the rising edge of the serial clock into a serial 20-bit shift register with the MSB first. See the PLL synthesizer and DC Clock Programming Table for details. The serial register is always active when the LE pin is held low. On the rising edge of the LE pin, the serial register is loaded and latched into the addressed registers for the particular function. The two least significant bits address the intended register for loading the serial data. This interface has been designed for a minimum LE pulse width. There is no need to discontinue the clock during loading of the 4 intended registers.

**NOTE:** Upon a rising edge on LE, the HFA3783 PLL unlocks the loop during a random period varying from 0 to  $1/(\text{reference frequency})$ . Fast frequency hopping applications may be affected during this time.

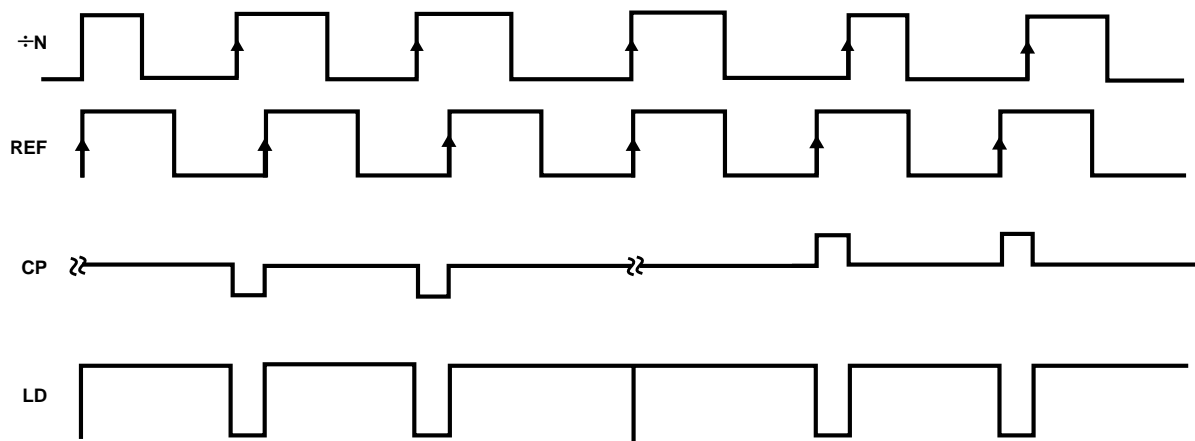


FIGURE 6. SIMPLIFIED CP AND LOCK DETECT OUTPUT WAVEFORMS

The four registers are as follows:

**R Counter:** Division factor “R” in binary weight format with R(0) as  $2^0$  and so on, for a decimal integer division ratio for the stable reference signal.

**A/B Counter:** A combination of binary weighted integer division factors for the “N” counter as explained by the relationship  $P*B+A$ .

**Operational Mode:** These register bits control the Charge Pump operation, Prescaler “P” setting, the power down feature of the PLL and the functions of the LD output pin.

**Offset Calibration:** These register bits control the division ratio, in binary weight, for the SAR clock and a special baseband output state for the Low Pass Filter.

**NOTE:** At power up ( $V_{CC}$  application), it is important to load the Operational Mode register before any sequence of the remaining registers.

### **Operational Modes Description**

**Bit M(0):** This bit is normally set at one for the PLL operation. Setting to zero can save up to 6mA of supply current by disabling the PLL, although the serial interface is always active for loading data. This operational mode bit controls the serial interface at power up and it is important to be loaded first, after application of  $V_{CC}$ .

**Bit M(2):** Selects the prescaler “P” for either 16 or 32.

**Bits M(3),M(4):** These bits select the desired Charge Pump current from 250 $\mu$ A to 1mA in four steps.

**Bits M(5), M(6):** Programming 00 will set the Charge Pump to “source” current when the VCO frequency is below the desired frequency. It is used for VCO’s where the frequency increases with increase in the voltage control. Programming 01 sets the Charge Pump to sink current when the VCO frequency is below the desired frequency. It is used for VCO’s where the frequency increases with decrease in the voltage control (Negative KVCO).

**Bits M(8), M(7) and M(13):** These bits define the LD output multiple operation. During the lock detect operation, the LD output follows the phase comparator output and can be used with external integration, as a frequency lock monitor function. LD output can be shorted to ground or used as a monitor pin for either the output of the “R” counter divider or the  $[P*B+A]$  dual modulus divider. In addition, it can be used as the serial register read back for testing purposes in a FIFO mode (not the latched register/counters themselves) by reading the MSB on the falling edge of LE and the remaining bits on the rising CLK edges.

**Bits M(14), M(15):** These bits set the Charge Pump operation for normal operation, constant sink or source and in a high impedance state. The high impedance state allows for external control.

### **DC Offset Calibration Counter Description**

**Bits C(0) to C(6):** Set a binary weighted decimal integer number for the stable reference input frequency division ratio. The ratio is used by the SAR for DC Offset Calibration in the HFA3783 and previously described in the Low Pass Filters section of this document.

**Bit C(11):** Enables a DC hold circuit which allows AC coupling of the baseband signals to a processor A/D’s. A common mode voltage applied to the baseband outputs during transmit mode switching reduces the coupling capacitors charging times.

### **Quadrature Modulator**

The differential baseband signals for the HFA3783 modulator require a controlled common mode voltage for proper operation of the device. Carrier suppression is consequently a function of the common mode DC match between the differential legs of each of the “I” and “Q” channels. The modulator bandwidth is very wide and need to be limited by external means. The inputs are equivalent to driving the up conversion quadrature mixers directly; therefore provisions for shaping the baseband signals before up conversion have to be made externally. Shaping can be accomplished either by an external filter or by pre-shaping in a baseband processor. Baseband signals up to 500mVpp differential can be used at the “I” and “Q” ports.

Centered upon a common mode voltage, the 500mVpp pre-shaped differential signals were used for the compression characteristics specified in this document. By reducing the magnitude of these signals improved low distortion modulation characteristics can be realized. The quiescent current for the upconversion mixers is established by the common mode input DC signal. By setting the common mode voltage to zero during the receive mode, power dissipation and mixer noise in the transmit path is reduced. The common mode voltage, routed through the baseband processor for temperature and  $V_{CC}$  tracking, is normally established by the HFA3783’s on board 1.2V reference. This reference is inactive during the power down mode.

The quadrature up converter mixers are also of a doubly balanced design. “I” and “Q” up converter signals are summed and buffered to drive the next stage, the AGC amplifier. As with the demodulators, both modulator mixers are driven from the same quadrature LO generator. These mixers feature a phase balance of  $\pm 2^\circ$  and amplitude balance of 0.5dB from 70 to 600MHz. These qualities are reflected into the SSB characteristics. For differential “I” and “Q”, 100KHz sinusoidal inputs of 375mVpp,  $90^\circ$  apart, the carrier feedthrough is typical -43dBc with typical sideband suppression of 43dBc at 374MHz.

A differential open collector linear output AGC amplifier with 70dB of dynamic range follows the mixers. This amplifier is based in a tight controlled voltage and temperature current

steering mechanism for gain control. The amplifier main function is controlling the power output of the transmit signal and has very linear AGC characteristics as shown in Figure 35. The differential open collector outputs require  $V_{CC}$  biasing as with any open collector application and exhibit high isolation. The HFA3783 output impedance is constant whether in the receive or transmit mode. Consequently, a combination matching network with the use of a single SAW filter can be used for both halves of the duplex operation. Single ended operation is discouraged due to; TX and RX return loss variation, loss of power output and lack of cancellation of PLL induced spurious signals. Differential summing match networks are strongly recommended when using single end SAW devices. S parameters for the output port are available in the S Parameter Tables section.

The AGC amplifier feature an output compression level of  $1V_{P-P}$ , with a cascaded performance capable of generating a typical CW power of  $-10\text{dBm}$  into  $250\Omega$  when differential inputs of  $250\text{mV DC}$  are applied to both "I" and "Q" inputs.

### IF interface

Both modulator and demodulator of the HFA3783 AC Cascaded Specifications in this document were characterized in a  $250\Omega$  system. The high impedance of the receive input and the open collector output structure of the transmit channel permit the use of a combination match network capable of interfacing with only one differential filter device in duplex operation. In addition, the HFA3783 input and output impedances have small variations when the device changes its mode of operation from transmit to receive. The system impedance ( $250\Omega$ ) is defined by the filter input/output impedance including its own match networks and this value has been chosen as a compromise between current consumption, voltage swing and therefore compression. A higher system  $Z_o$  can compromise the voltage swing capabilities due to the low voltage operation of the HFA3783 and a low system  $Z_o$  affects the power supply current consumed by the application in general, for the same RF power budget.

The output match network of the transmit output, includes a differential "L" match network used to bias the differential collectors which are of high impedance. This high impedance is lowered to a value of around  $2K\Omega$  by a parallel resistor placed across the collector terminals. This value sets the output impedance of the two collectors and also serves as a compromise value for the loaded "Q" of the network for a desired system bandwidth. The other side of the match network is set to match  $250\Omega$  (from a filter match application) and is directly connected to the receive differential terminals; therefore presenting a controlled termination to the high input impedance port of the receive AGC. The use of DC blocking capacitors is needed to avoid a DC path between the HFA3783 receive terminals and is

maybe optional depending of the differential network used to match an external filter to a  $250\Omega$  system.

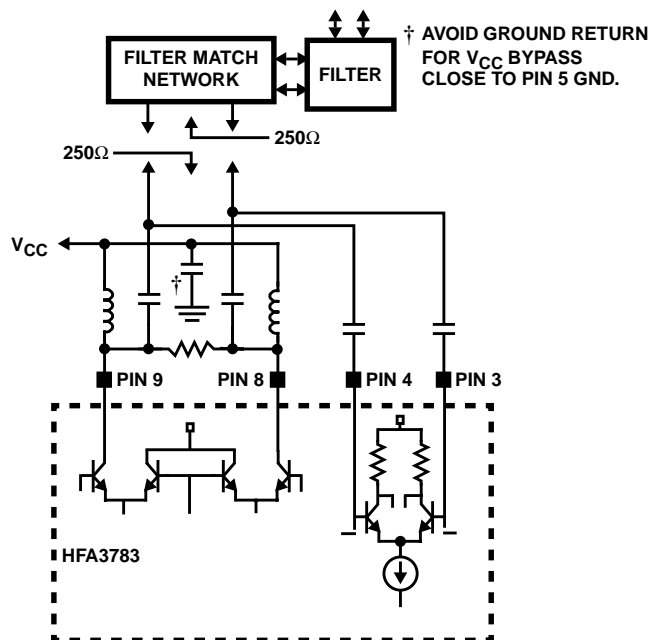


FIGURE 7. SIMPLIFIED IF INPUT/OUTPUT COMBINED MATCH NETWORK

As with any differential network, symmetry is paramount. The use of matched length lines and good differential isolation, helps the structure reject common mode induced signals from other parts of the system. Special attention to the collector outputs is necessary to reject  $V_{CC}$  induced spurious signals and to reject internally induced PLL spurious tones. Although the network topology is simple theoretically, its implementation is challenged by layout routing and parasitics which have to be taken into consideration.

Typical Performance Curves

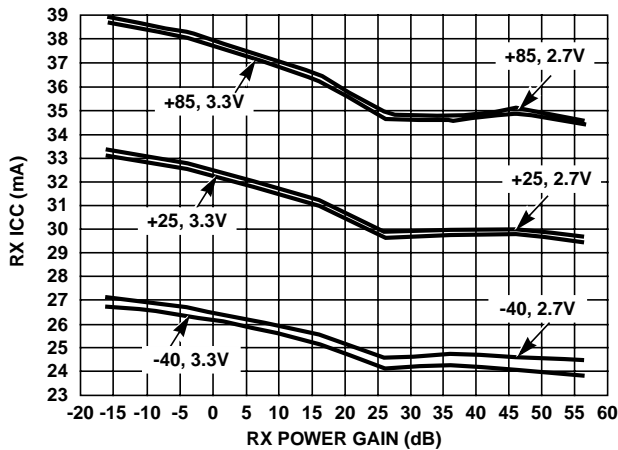


FIGURE 8. RX ICC vs POWER GAIN OVER TEMPERATURE

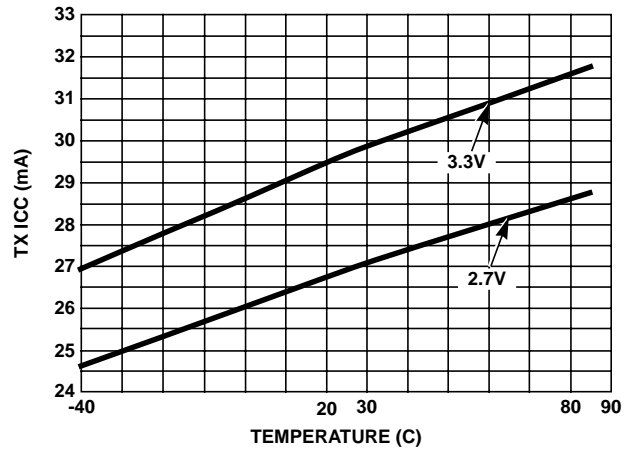


FIGURE 9. TX ICC WITH TXI/Q = 1.3V OVER TEMPERATURE AND VOLTAGE

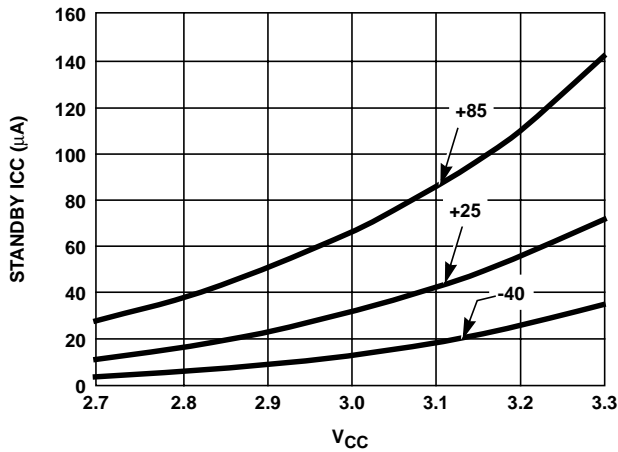


FIGURE 10. STANDBY ICC vs V<sub>CC</sub>

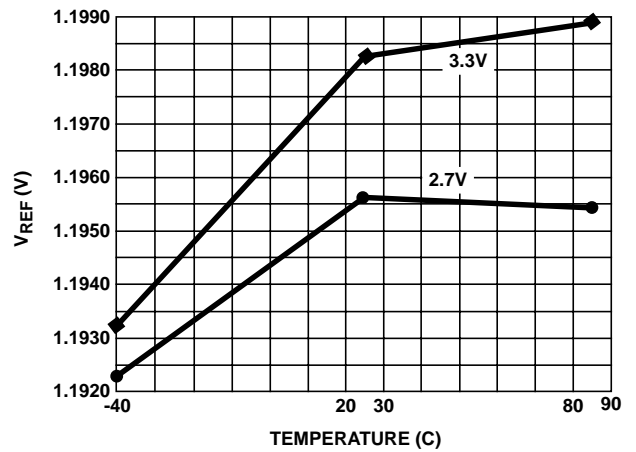


FIGURE 11. 1.2V V<sub>REF</sub> VOLTAGE OVER V<sub>CC</sub> AND TEMPERATURE

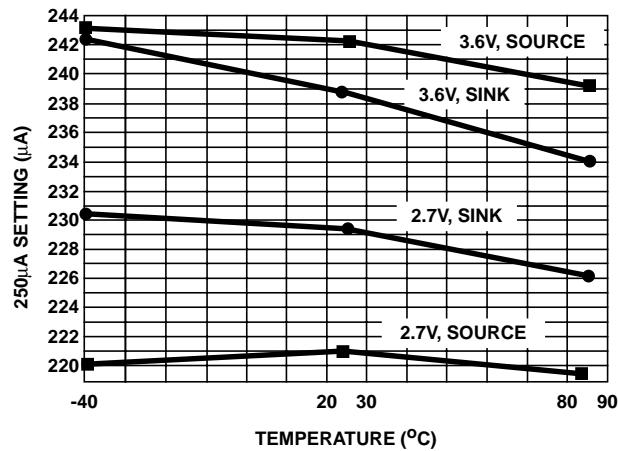


FIGURE 12. CHARGE PUMP 250 $\mu$ A SETTING SINK AND SOURCE CURRENT OVER TEMPERATURE AND VOLTAGE

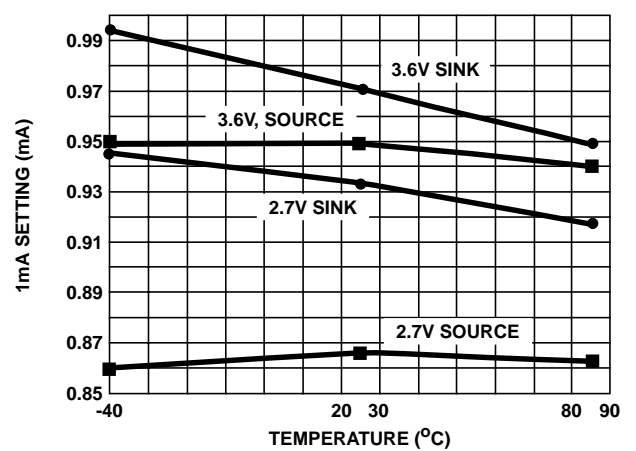


FIGURE 13. CHARGE PUMP 1mA SETTING SINK AND SOURCE CURRENT OVER TEMPERATURE AND VOLTAGE

Typical Performance Curves (Continued)

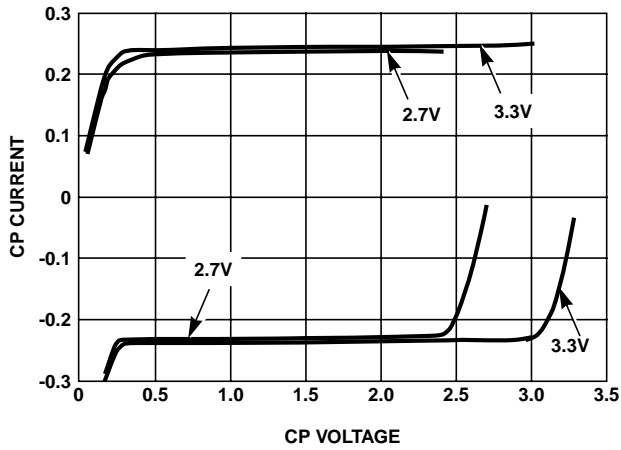


FIGURE 14. CHARGE PUMP CHARACTERISTICS AT 250µA

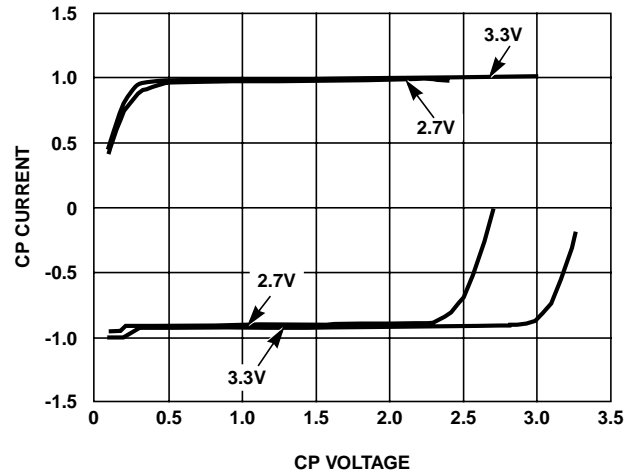


FIGURE 15. CHARGE PUMP CHARACTERISTICS AT 1mA

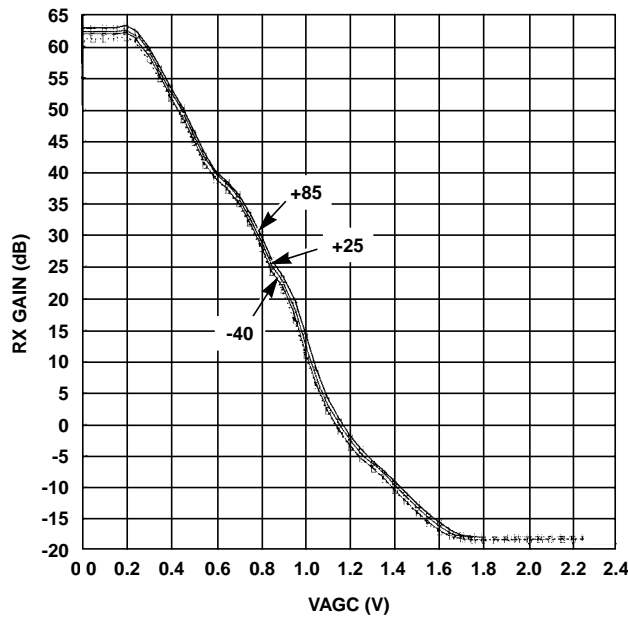


FIGURE 16. RX AGC POWER GAIN vs VAGC OVER TEMPERATURE AT ALL V<sub>CC</sub>

Typical Performance Curves (Continued)

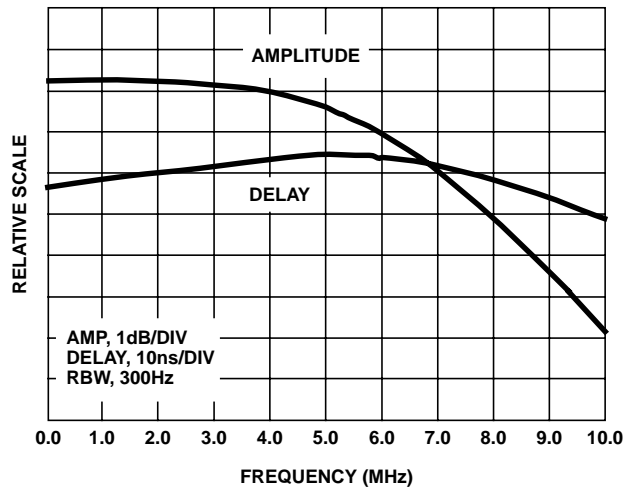


FIGURE 17. RX BASEBAND LPF PROFILE

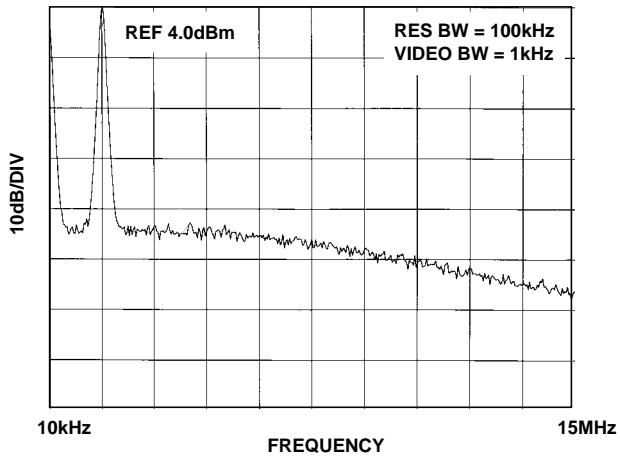


FIGURE 18. RX BASEBAND SPECTRUM, TONE AT 1.5MHz  
POWER GAIN OF 56dB. OUTPUT CONVERTED  
TO SINGLE ENDED 50Ω

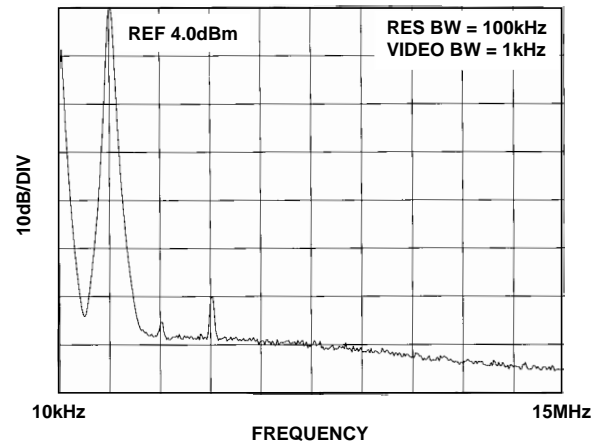


FIGURE 19. RX BASEBAND SPECTRUM, TONE AT 1.5MHz  
POWER GAIN OF -16dB. OUTPUT CONVERTED  
TO SINGLE ENDED 50Ω

Typical Performance Curves (Continued)

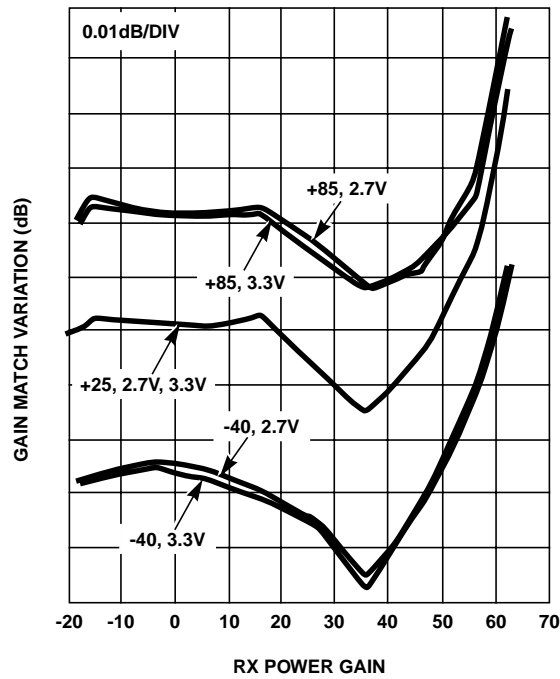


FIGURE 20. RX I/Q CHANNEL GAIN MATCH vs POWER OVER TEMPERATURE AND  $V_{CC}$

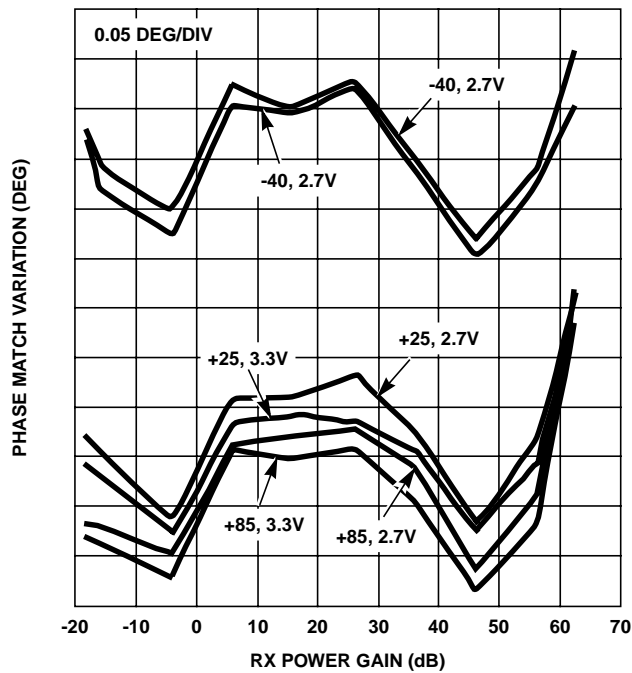


FIGURE 21. RX I, Q CHANNEL PHASE MATCH vs POWER GAIN OVER TEMPERATURE AND  $V_{CC}$



Typical Performance Curves (Continued)

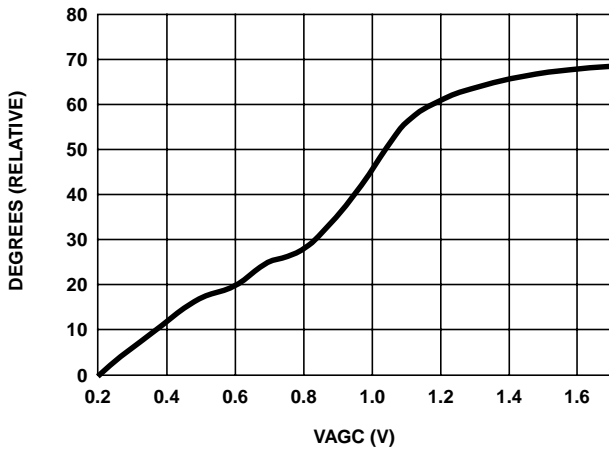


FIGURE 22. RX INSERTION PHASE vs VAGC

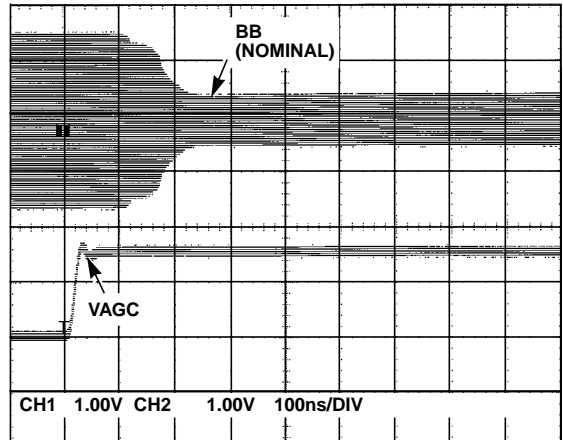


FIGURE 23. RX BASEBAND AGC RESPONSE TIME, 0dBm INPUT

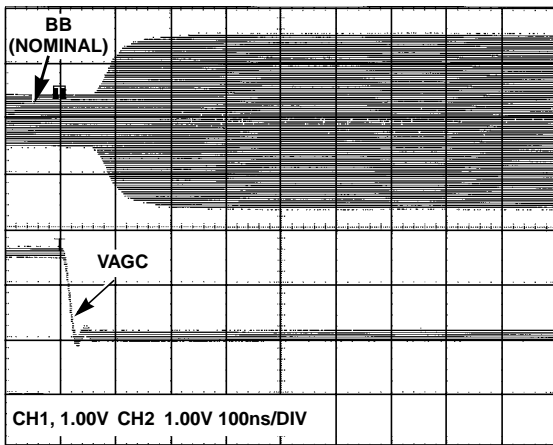


FIGURE 24. RX BASEBAND AGC RESPONSE TIME, 0dBm INPUT

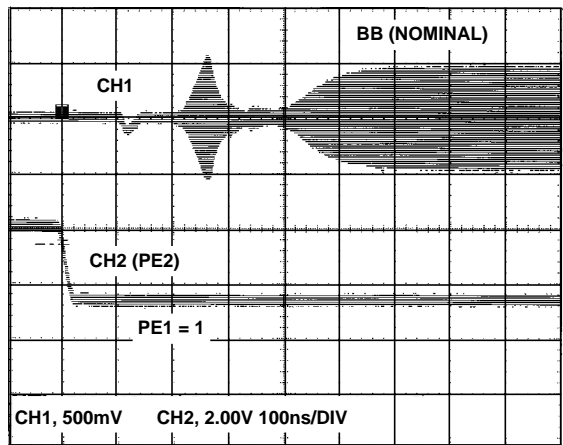


FIGURE 25. TX TO RX BASEBAND SWITCHING TIME

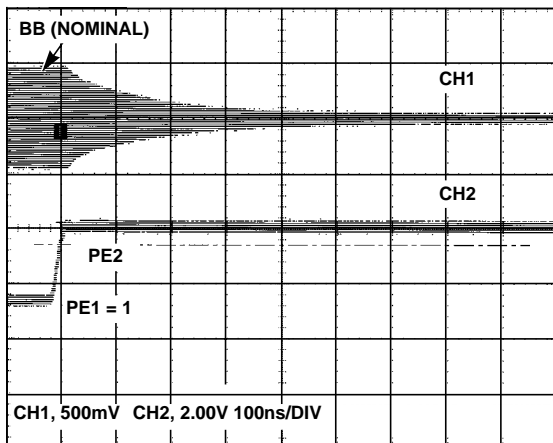


FIGURE 26. RX TO TX BASEBAND SWITCHING TIME

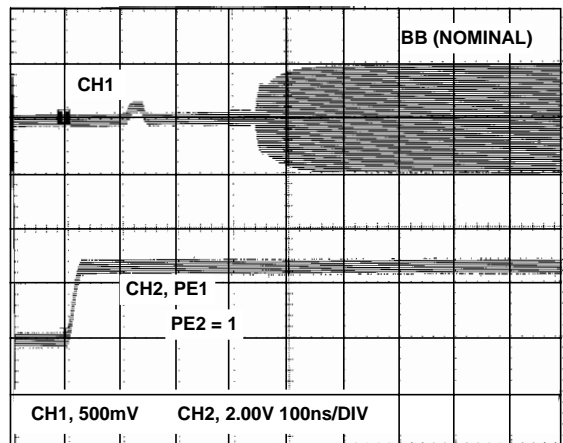


FIGURE 27. RX BASEBAND AT POWER UP

Typical Performance Curves (Continued)

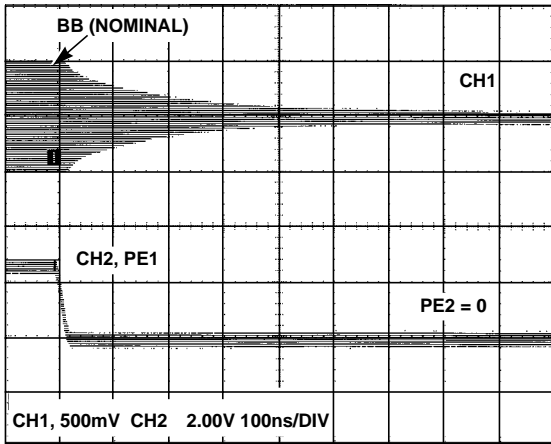


FIGURE 28. RX BASEBAND AT POWER DOWN

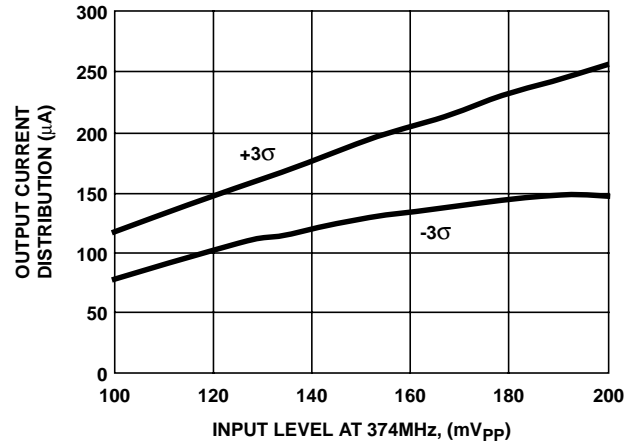


FIGURE 29. IF DETECTOR OUTPUT CURRENT,  $\pm 3$  SIGMA DISTRIBUTION AT ALL TEMPERATURE AND  $V_{CC}$

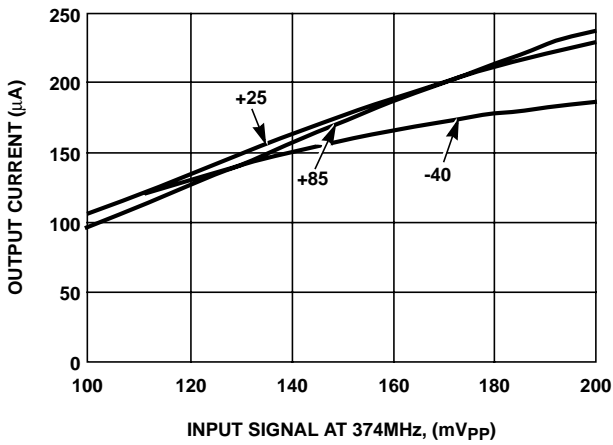


FIGURE 30. TYPICAL IF DETECTOR OUTPUT CURRENT AT ALL  $V_{CC}$

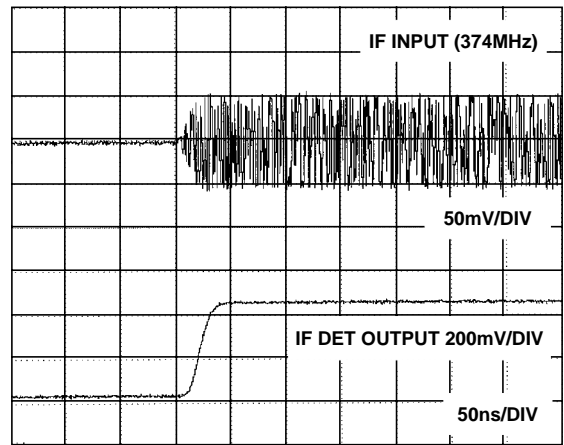


FIGURE 31. IF DETECTOR RESPONSE, RISE TIME

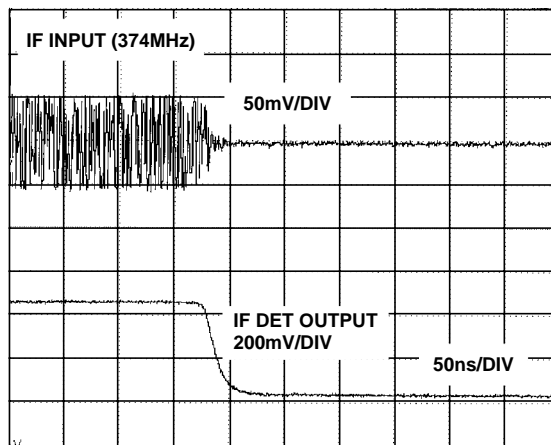


FIGURE 32. IF DETECTOR RESPONSE, FALL TIME

Typical Performance Curves (Continued)

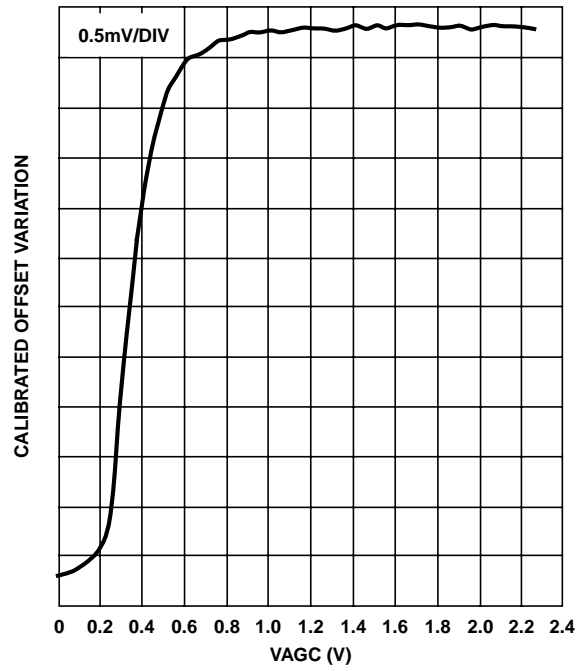


FIGURE 33. BASEBAND OUTPUT OFFSET VOLTAGE VARIATION vs VAGC, IF = 0V

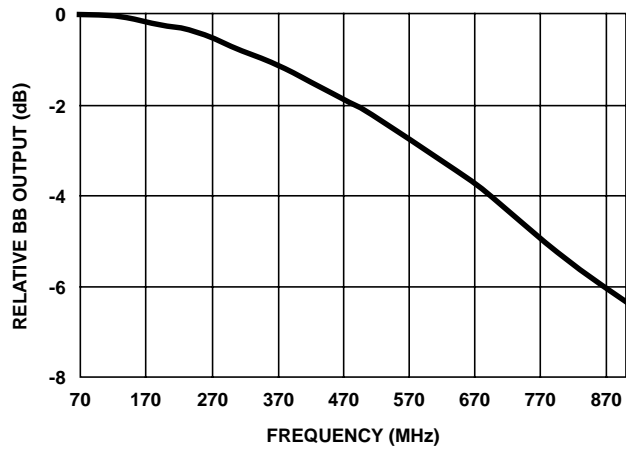


FIGURE 34. CASCADED RX FREQUENCY RESPONSE, BB AT 1MHz

Typical Performance Curves (Continued)

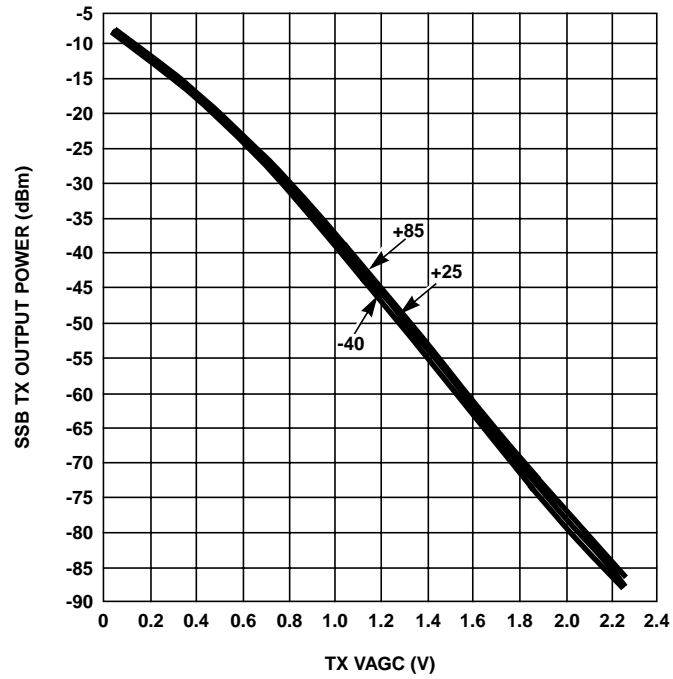


FIGURE 35. TX POWER OUT vs TX VAGC OVER TEMPERATURE AT ALL V<sub>CC</sub>

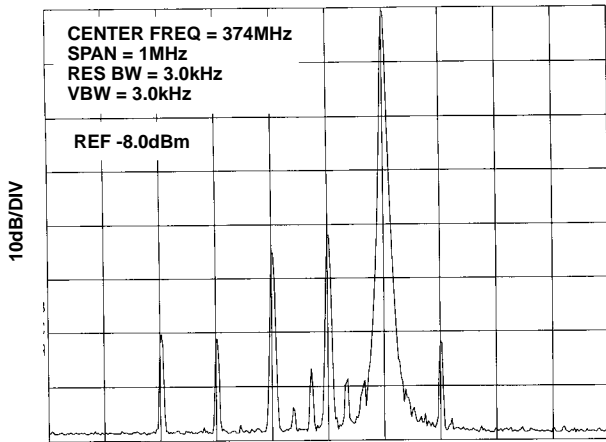


FIGURE 36. TX SSB OUTPUT CHARACTERISTICS AT FULL GAIN

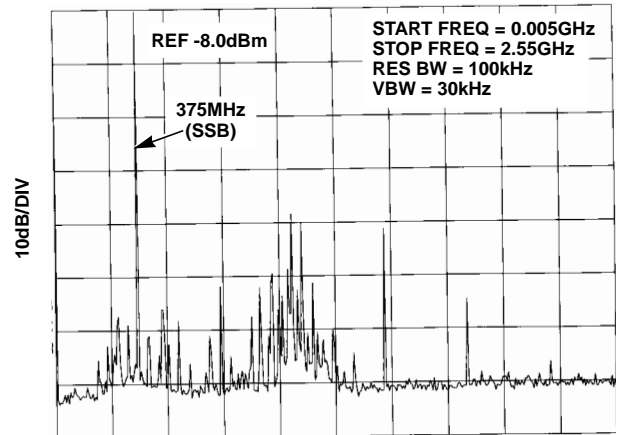


FIGURE 37. TX SSB OUTPUT CHARACTERISTICS AT FULL GAIN AND WIDE SPECTRUM WITH MATCH NETWORK

Typical Performance Curves (Continued)

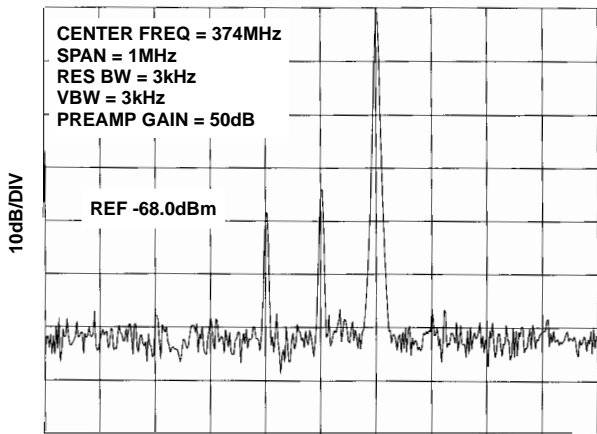


FIGURE 38. TX SSB OUTPUT CHARACTERISTICS AT -60dB FROM FULL GAIN

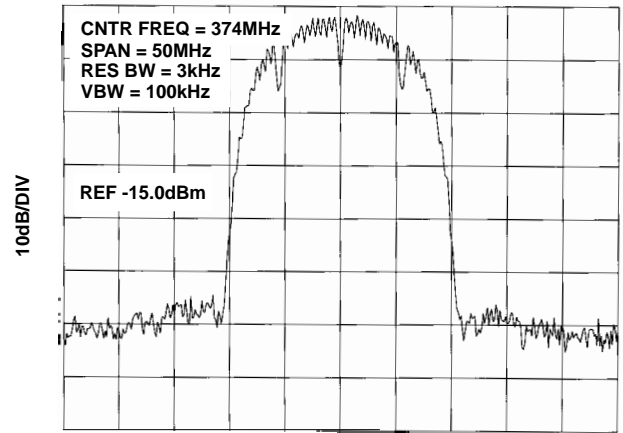


FIGURE 39. TX SPREAD SPECTRUM OUTPUT CHARACTERISTICS AT FULL GAIN, BB INPUTS AT 500mV<sub>pp</sub>

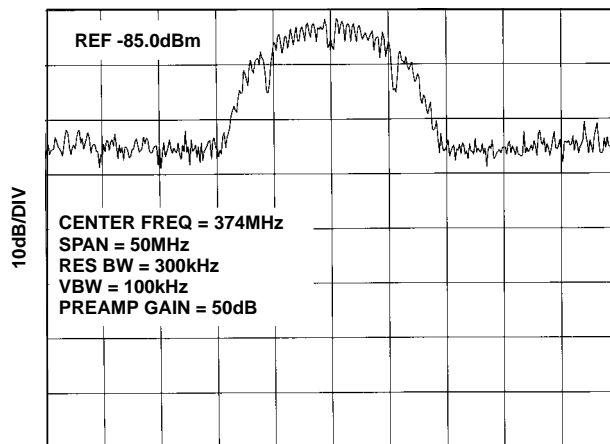


FIGURE 40. TX SPREAD SPECTRUM OUTPUT CHARACTERISTICS AT -70dB FROM FULL GAIN, BB INPUTS AT 500mV<sub>pp</sub>

Typical Performance Curves (Continued)

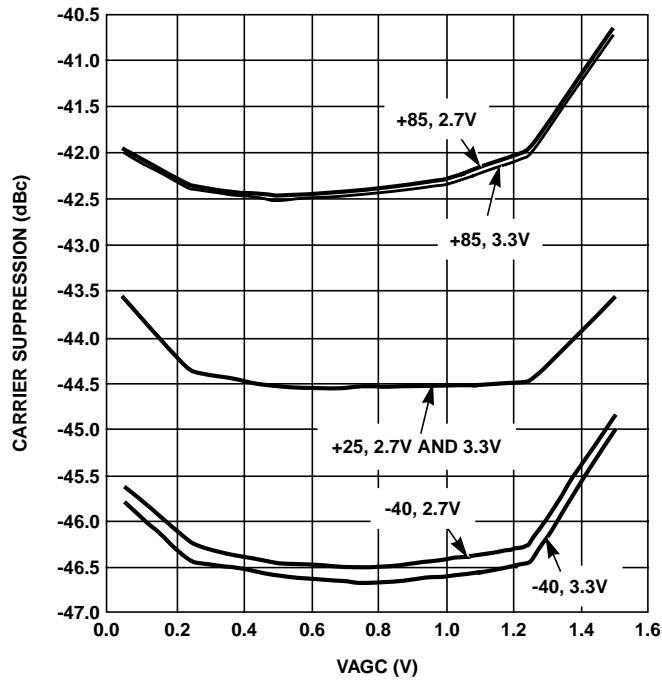


FIGURE 41. TYPICAL TX CARRIER SUPPRESSION vs VAGC OVER TEMPERATURE

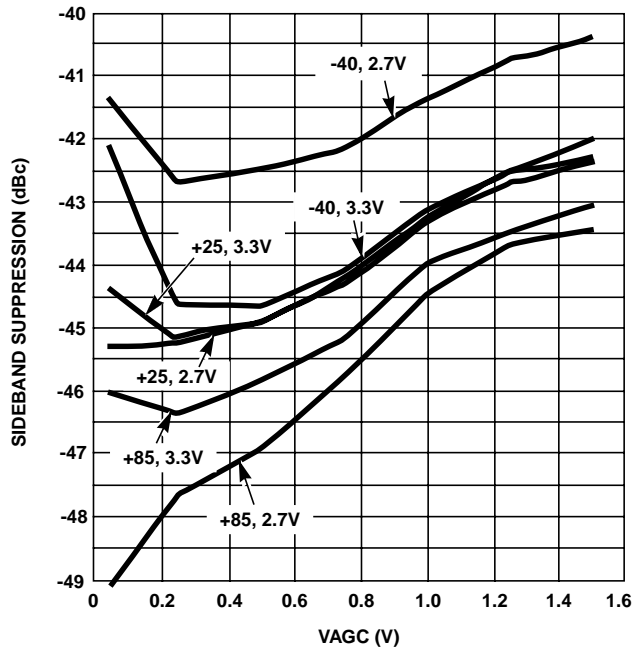


FIGURE 42. TYPICAL TX LOWER SIDE BAND SUPPRESSION vs VAGC OVER TEMPERATURE

Typical Performance Curves (Continued)

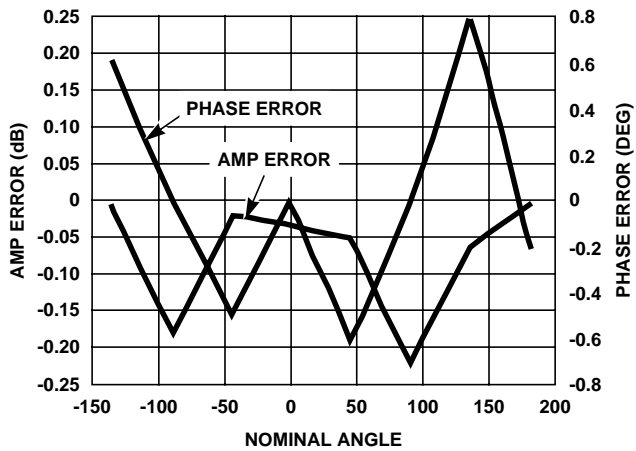


FIGURE 43. TYPICAL TX CARRIER STATIC AMPLITUDE AND PHASE BALANCE AT 250mV DC DIFFERENTIAL BB INPUTS

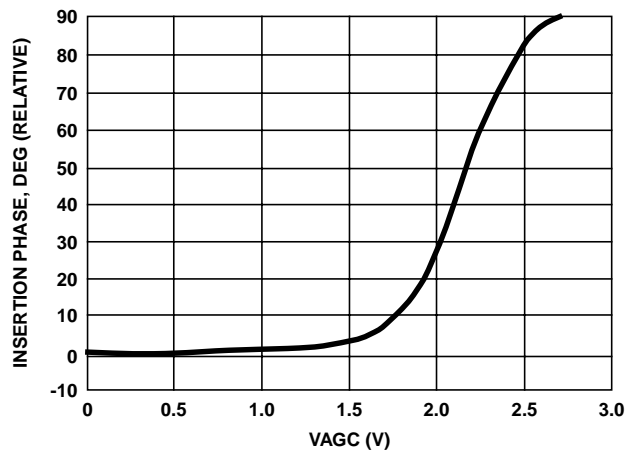


FIGURE 44. TX INSERTION PHASE vs VAGC

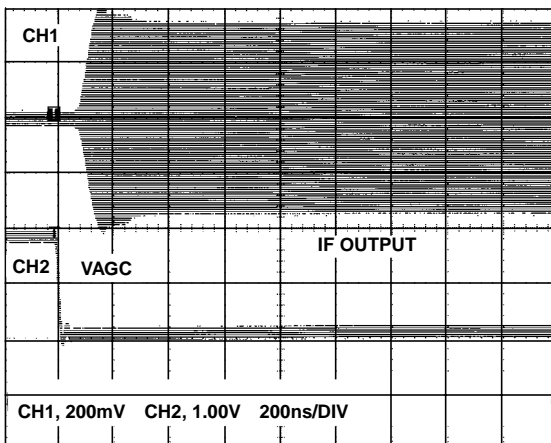


FIGURE 45. TX AGC RESPONSE TIME, FULL GAIN

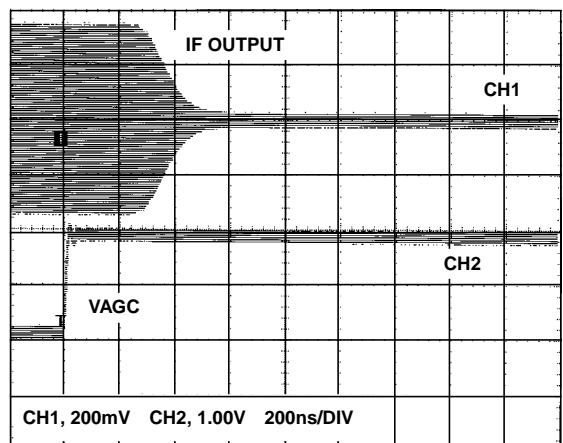


FIGURE 46. TX AGC RESPONSE TIME, FULL GAIN

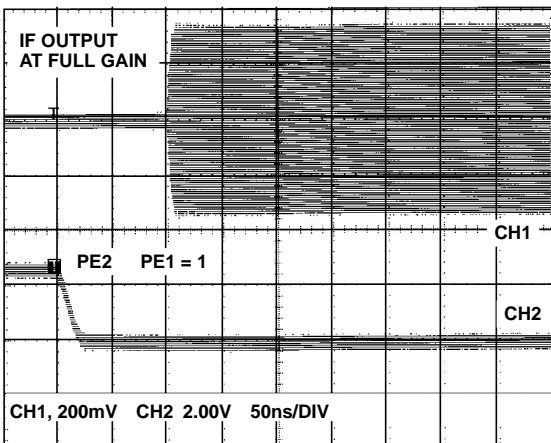


FIGURE 47. RX TO TX IF OUTPUT SWITCHING TIME

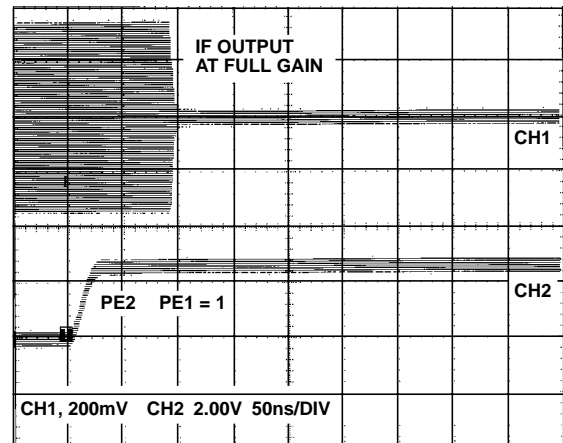


FIGURE 48. TX TO RX IF OUTPUT SWITCHING TIME

Typical Performance Curves (Continued)

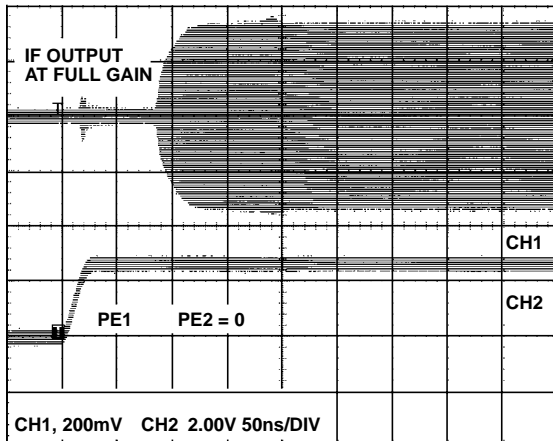


FIGURE 49. TX IF OUTPUT AT POWER UP

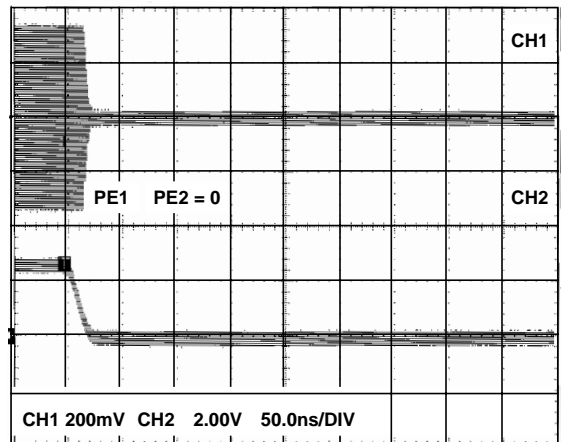


FIGURE 50. TX IF OUTPUT AT POWER DOWN

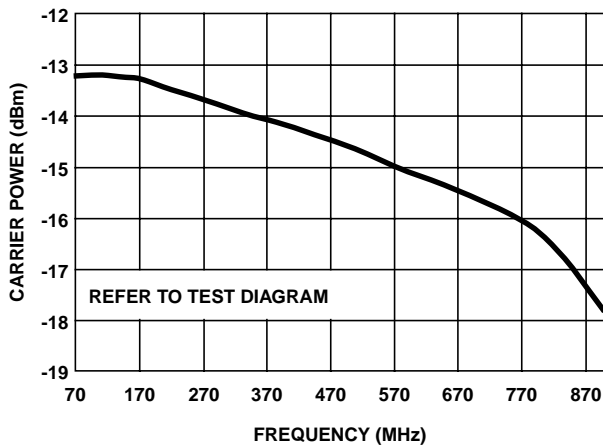


FIGURE 51. TX OUT POWER vs FREQUENCY, BB AT DC

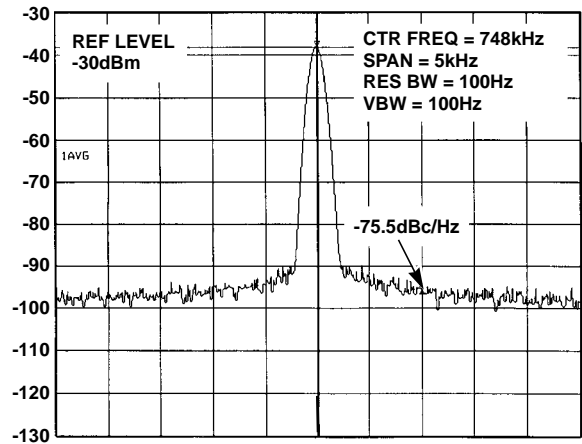


FIGURE 52. EVAL BOARD TYPICAL SYNTHESIZER CLOSE IN PHASE NOISE

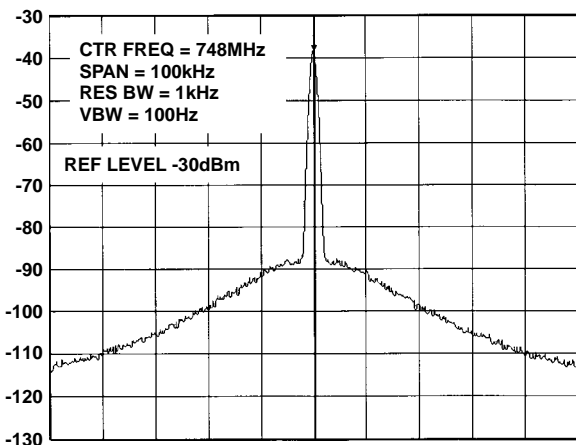


FIGURE 53. EVAL BOARD TYPICAL SYNTHESIZER OUTPUT WITH PLL AT 10kHz BW

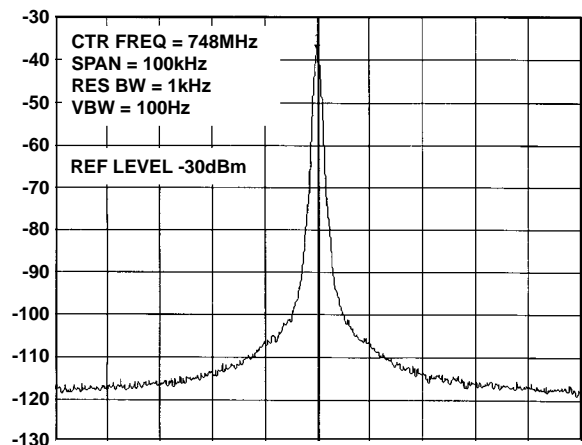


FIGURE 54. EVAL BOARD TYPICAL SYNTHESIZER OUTPUT WITH PLL AT 1kHz BW



Typical Performance Curves (Continued)

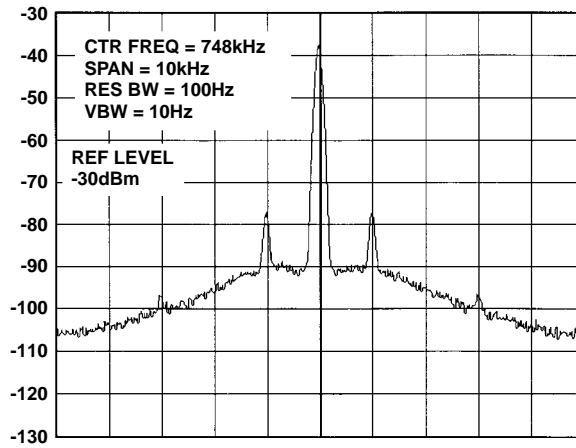
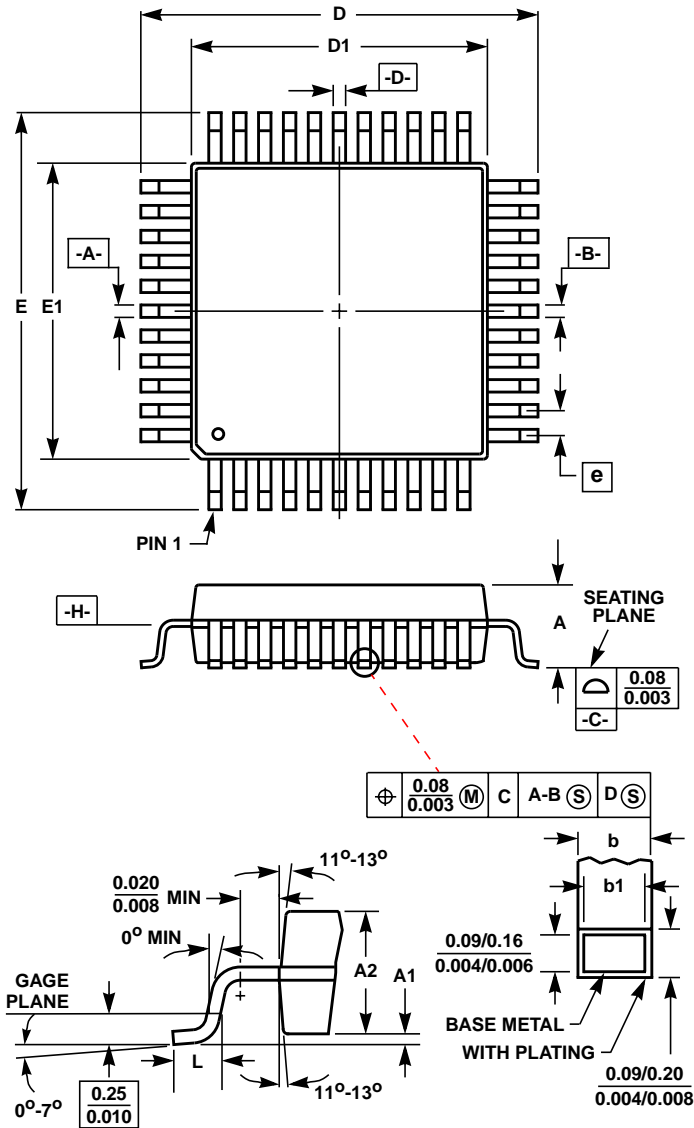


FIGURE 55. EVAL BOARD SYNTHESIZER TX TO RX SWITCHING SPURIOUS RESPONSE AT 1kHz SWITCHING FREQUENCY, PLL BW = 10kHz

Thin Plastic Quad Flatpack Packages (LQFP)



**Q48.7x7A (JEDEC MS-026BBC ISSUE B)**  
**48 LEAD THIN PLASTIC QUAD FLATPACK PACKAGE**

SYMBOL	INCHES		MILLIMETERS		NOTES
	MIN	MAX	MIN	MAX	
A	-	0.062	-	1.60	-
A1	0.002	0.005	0.05	0.15	-
A2	0.054	0.057	1.35	1.45	-
b	0.007	0.010	0.17	0.27	6
b1	0.007	0.009	0.17	0.23	-
D	0.350	0.358	8.90	9.10	3
D1	0.272	0.280	6.90	7.10	4, 5
E	0.350	0.358	8.90	9.10	3
E1	0.272	0.280	6.90	7.10	4, 5
L	0.018	0.029	0.45	0.75	-
N	48		48		7
e	0.020 BSC		0.50 BSC		-

Rev. 2 1/99

NOTES:

- Controlling dimension: MILLIMETER. Converted inch dimensions are not necessarily exact.
- All dimensions and tolerances per ANSI Y14.5M-1982.
- Dimensions D and E to be determined at seating plane  $\square$ -C-.
- Dimensions D1 and E1 to be determined at datum plane  $\square$ -H-.
- Dimensions D1 and E1 do not include mold protrusion. Allowable protrusion is 0.25mm (0.010 inch) per side.
- Dimension b does not include dambar protrusion. Allowable dambar protrusion shall not cause the lead width to exceed the maximum b dimension by more than 0.08mm (0.003 inch).
- "N" is the number of terminal positions.

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